TECHNOLOGY

## 24-Bit $\Delta \Sigma$ ADC with Easy Drive Input Current Cancellation and $I^{2} C$ Interface

## FEATURES

- Easy Drive ${ }^{\text {TM }}$ Technology Enables Rail-to-Rail Inputs with Zero Differential Input Current
- Directly Digitizes High Impedance Sensors with Full Accuracy
- GND to V $\operatorname{CC}$ Input/Reference Common Mode Range
- 2-Wire ${ }^{2} \mathrm{C}$ Interface
- Programmable $50 \mathrm{~Hz}, 60 \mathrm{~Hz}$ or Simultaneous $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ Rejection Mode
- 2ppm (0.25LSB) INL, No Missing Codes
- 1ppm Offset and 15ppm Full-Scale Error
- Selectable 2x Speed Mode
- No Latency: Digital Filter Settles in a Single Cycle
- Single Supply 2.7 V to 5.5 V Operation
- Internal Oscillator
- Six Addresses Available and One Global Address for Synchronization
- Available in a Tiny ( $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ ) 10-Lead DFN Package


## APPLICATIONS

- Direct Sensor Digitizer
- Weight Scales
- Direct Temperature Measurement
- Strain Gauge Transducers
- Instrumentation
- Industrial Process Control
- DVMs and Meters


## DESCRIPTION

The LTC ${ }^{\circledR} 2485$ combines a 24 -bit plus sign No Latency $\Delta \Sigma^{\top M}$ analog-to-digital converter with patented Easy Drive technology and ${ }^{2} \mathrm{C}$ digital interface. The patented sampling scheme eliminates dynamic input current errors and the shortcomings of on-chip buffering through automatic cancellation of differential input current. This allows large external source impedances and input signals, with rail-torail input range to be directly digitized while maintaining exceptional DC accuracy.
The LTC2485 includes an on-chip oscillator. The LTC2485 can be configured through an $I^{2} \mathrm{C}$ interface to reject line frequencies. $50 \mathrm{~Hz}, 60 \mathrm{~Hz}$ or simultaneous $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ line frequency rejection can be selected as well as a $2 x$ speed-up mode.
The LTC2485 allows a wide common mode input range ( 0 V to $\mathrm{V}_{\mathrm{CC}}$ ) independent of the reference voltage. The reference can be as low as 100 mV or can be tied directly to $V_{\text {CC }}$. The LTC2485 includes an on-chip trimmed oscillator eliminating the need for external crystals or oscillators. Absolute accuracy and low drift are automatically maintained through continuous, transparent, offset and full-scale calibration.
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## TYPICAL APPLICATION




## ABSOLUTE MAXIMUM RATIOGS

(Notes 1, 2)
Supply Voltage ( $\mathrm{V}_{\text {CC }}$ ) to GND ...................... -0.3 V to 6V
Analog Input Voltage to GND ....... -0.3 V to $\left(\mathrm{V}_{\text {CC }}+0.3 \mathrm{~V}\right)$
Reference Input Voltage to GND .. -0.3 V to ( $\mathrm{V}_{\mathrm{CC}}+0.3 \mathrm{~V}$ )
Digital Input Voltage to GND ....... - 0.3 V to ( $\mathrm{V}_{\mathrm{CC}}+0.3 \mathrm{~V}$ )
Digital Output Voltage to GND...... -0.3 V to $\left(\mathrm{V}_{C C}+0.3 \mathrm{~V}\right)$
Operating Temperature Range
LTC2485C $\qquad$ $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$
LTC2485I ................................................ $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$
Storage Temperature Range $\qquad$ $-65^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$

## PIn CONFIGURATIOn



10-LEAD ( $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ ) PLASTIC DFN
$T_{\mathrm{JMAX}}=125^{\circ} \mathrm{C}, \theta_{\mathrm{JA}}=43^{\circ} \mathrm{C} / \mathrm{W}$
EXPOSED PAD (PIN 11) IS GND, MUST BE SOLDERED TO PCB

## ORDER InFORMATION

| LEAD FREE FINISH | TAPE AND REEL | PART MARKING* | PACKAGE DESCRIPTION | TEMPERATURE RANGE |
| :--- | :--- | :--- | :--- | :--- |
| LTC2485CDD\#PBF | LTC2485CDD\#TRPBF | LBST | 10 -Lead $(3 \mathrm{~mm} \times 3 \mathrm{~mm})$ Plastic DFN | $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ |
| LTC2485IDD\#PBF | LTC2485IDD\#TRPBF | LBST | 10 -Lead $(3 \mathrm{~mm} \times 3 \mathrm{~mm})$ Plastic DFN | $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ |

Consult LTC Marketing for parts specified with wider operating temperature ranges. *The temperature grade is identified by a label on the shipping container.
For more information on lead free part marking, go to: http://www.linear.com/leadfree/
For more information on tape and reel specifications, go to: http://www.linear.com/tapeandreel/

ELECTRICRL CHARACTERSTCS (ПORMPLSPEEP) The © denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. (Notes 3,4 )

| PARAMETER | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Resolution (No Missing Codes) | $0.1 \leq \mathrm{V}_{\text {REF }} \leq \mathrm{V}_{\text {CC }},-\mathrm{FS} \leq \mathrm{V}_{\text {IN }} \leq+\mathrm{FS}$ (Note 5) | $\bullet$ | 24 |  |  | Bits |
| Integral Nonlinearity | $\begin{aligned} & 5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CC}} \leq 5.5 \mathrm{~V}, \mathrm{~V}_{\text {REF }}=5 \mathrm{~V}, \mathrm{~V}_{\text {IN (CM }}=2.5 \mathrm{~V} \text { (Note 6) } \\ & 2.7 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CC}} \leq 5.5 \mathrm{~V}, \mathrm{~V}_{\text {REF }}=2.5 \mathrm{~V}, \mathrm{~V}_{\text {IN(CM) }}=1.25 \mathrm{~V} \text { (Note 6) } \end{aligned}$ | $\bullet$ |  | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | 10 | $\begin{aligned} & \text { ppm of } V_{\mathrm{REF}} \\ & \mathrm{ppm} \text { of } V_{\mathrm{REF}} \end{aligned}$ |
| Offset Error | $2.5 \mathrm{~V} \leq \mathrm{V}_{\text {REF }} \leq \mathrm{V}_{\text {CC }}, \mathrm{GND} \leq \mathrm{IN}^{+}=\mathrm{IN}^{-} \leq \mathrm{V}_{\text {CC }}$ (Note 13) | $\bullet$ |  | 0.5 | 2.5 | $\mu \mathrm{V}$ |
| Offset Error Drift | $2.5 \mathrm{~V} \leq \mathrm{V}_{\text {REF }} \leq \mathrm{V}_{\text {CC }}, \mathrm{GND} \leq \mathrm{IN}^{+}=\mathrm{IN}^{-} \leq \mathrm{V}_{\text {CC }}$ |  |  | 10 |  | $\mathrm{nV} /{ }^{\circ} \mathrm{C}$ |
| Positive Full-Scale Error | $2.5 \mathrm{~V} \leq \mathrm{V}_{\text {REF }} \leq \mathrm{V}_{\text {CC }}, \mathrm{IN}^{+}=0.75 \mathrm{~V}_{\text {REF }}, \mathrm{IN}^{-}=0.25 \mathrm{~V}_{\text {REF }}$ | $\bullet$ |  |  | 25 | ppm of $\mathrm{V}_{\text {REF }}$ |
| Positive Full-Scale Error Drift | $2.5 \mathrm{~V} \leq \mathrm{V}_{\text {REF }} \leq \mathrm{V}_{\text {CC }}, \mathrm{IN}^{+}=0.75 \mathrm{~V}_{\text {REF }}, \mathrm{IN}^{-}=0.25 \mathrm{~V}_{\text {REF }}$ |  |  | 0.1 |  | ppm of $\mathrm{V}_{\text {REF }} /{ }^{\circ} \mathrm{C}$ |
| Negative Full-Scale Error | $2.5 \mathrm{~V} \leq \mathrm{V}_{\text {REF }} \leq \mathrm{V}_{\text {CC }}, \mathrm{IN}^{-}=0.75 \mathrm{~V}_{\text {REF }}, \mathrm{IN}^{+}=0.25 \mathrm{~V}_{\text {REF }}$ | $\bullet$ |  |  | 25 | ppm of $\mathrm{V}_{\text {REF }}$ |
| Negative Full-Scale Error Drift | $2.5 \mathrm{~V} \leq \mathrm{V}_{\text {REF }} \leq \mathrm{V}_{\text {CC }}, \mathrm{IN}^{-}=0.75 \mathrm{~V}_{\text {REF }}, \mathrm{IN}^{+}=0.25 \mathrm{~V}_{\text {REF }}$ |  |  | 0.1 |  | ppm of $\mathrm{V}_{\text {REF }} /{ }^{\circ} \mathrm{C}$ |
| Total Unadjusted Error |  |  |  | $\begin{aligned} & 15 \\ & 15 \\ & 15 \end{aligned}$ |  | ppm of $V_{\text {REF }}$ ppm of $V_{\text {REF }}$ ppm of $V_{\text {REF }}$ |
| Output Noise | $5 \mathrm{~V} \leq \mathrm{V}_{\text {CC }} \leq 5.5 \mathrm{~V}, \mathrm{~V}_{\text {REF }}=5 \mathrm{~V}, \mathrm{GND} \leq \mathrm{IN}^{-}=\mathrm{IN}^{+} \leq \mathrm{V}_{\text {CC }}$ (Note 12) |  |  | 0.6 |  | $\mu \mathrm{V}_{\text {RMS }}$ |
| Internal PTAT Signal | $\mathrm{T}_{\mathrm{A}}=27^{\circ} \mathrm{C}$ |  | 390 |  | 450 | mV |

# ELECTRICAL CHARACTERISTICS (2X SPEED) The • denotes the specifications which apply over 

the full operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. (Notes 3, 4)
$\left.\begin{array}{l|l|l|c|r}\hline \text { PARAMETER } & \text { CONDITIONS } & \text { MIN } & \text { TYP } & \text { MAX }\end{array}\right)$ UNITS

COחVERTER CHARACTERISTICS The • denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. (Notes 3, 4)

| PARAMETER | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input Common Mode Rejection DC | $2.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{REF}} \leq \mathrm{V}_{\mathrm{CC}}, \mathrm{GND} \leq \mathrm{IN}^{-}=\mathrm{IN}^{+} \leq \mathrm{V}_{\mathrm{CC}}$ (Note 5) | $\bullet$ | 140 |  |  | dB |
| Input Common Mode Rejection $50 \mathrm{~Hz} \pm 2 \%$ | $2.5 \mathrm{~V} \leq \mathrm{V}_{\text {REF }} \leq \mathrm{V}_{\text {CC }}, \mathrm{GND} \leq I \mathrm{~N}^{-}=1 \mathrm{~N}^{+} \leq \mathrm{V}_{\text {CC }}($ Note 5) | $\bullet$ | 140 |  |  | dB |
| Input Common Mode Rejection $60 \mathrm{~Hz} \pm 2 \%$ | $2.5 \mathrm{~V} \leq \mathrm{V}_{\text {REF }} \leq \mathrm{V}_{\text {CC }}, \mathrm{GND} \leq \mathrm{IN}^{-}=\mathrm{IN}^{+} \leq \mathrm{V}_{\text {CC }}($ Note 5) | $\bullet$ | 140 |  |  | dB |
| Input Normal Mode Rejection $50 \mathrm{~Hz} \pm 2 \%$ | $2.5 \mathrm{~V} \leq \mathrm{V}_{\text {REF }} \leq \mathrm{V}_{\text {CC }}, \mathrm{GND} \leq \mathrm{IN}^{-}=\mathrm{IN}^{+} \leq \mathrm{V}_{\text {CC }}($ Notes 5, 7) | $\bullet$ | 110 | 120 |  | dB |
| Input Normal Mode Rejection $60 \mathrm{~Hz} \pm 2 \%$ | $2.5 \mathrm{~V} \leq \mathrm{V}_{\text {REF }} \leq \mathrm{V}_{\text {CC }}, \mathrm{GND} \leq \mathrm{IN}^{-}=\mathrm{IN}^{+} \leq \mathrm{V}_{\text {CC }}($ Notes 5, 8) | $\bullet$ | 110 | 120 |  | dB |
| Input Normal Mode Rejection $50 \mathrm{~Hz} / 60 \mathrm{~Hz} \pm 2 \%$ | $2.5 \mathrm{~V} \leq \mathrm{V}_{\text {REF }} \leq \mathrm{V}_{\text {CC }}, \mathrm{GND} \leq \mathrm{IN}^{-}=\mathrm{IN}^{+} \leq \mathrm{V}_{\text {CC }}($ Notes 5, 9) | $\bullet$ | 87 |  |  | dB |
| Reference Common Mode Rejection DC | $2.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{REF}} \leq \mathrm{V}_{\mathrm{CC}}, \mathrm{GND} \leq \mathrm{IN}^{-}=\mathrm{IN}^{+} \leq \mathrm{V}_{\text {CC }}$ (Note 5) | $\bullet$ | 120 | 140 |  | dB |
| Power Supply Rejection DC | $\mathrm{V}_{\text {REF }}=2.5 \mathrm{~V}, \mathrm{IN}^{-}=1 \mathrm{IN}^{+}=\mathrm{GND}$ |  |  | 120 |  | dB |
| Power Supply Rejection, $50 \mathrm{~Hz} \pm 2 \%$ | $\mathrm{V}_{\text {REF }}=2.5 \mathrm{~V}, \mathrm{IN}^{-}=\mathrm{IN}^{+}=\mathrm{GND}$ (Notes 7, 9) |  |  | 120 |  | dB |
| Power Supply Rejection, $60 \mathrm{~Hz} \pm 2 \%$ | $\mathrm{V}_{\text {REF }}=2.5 \mathrm{~V}, \mathrm{IN}^{-}=\mathrm{IN}^{+}=\mathrm{GND}$ (Notes 8, 9) |  |  | 120 |  | dB |

A $A$ ALOG INPUT AחD REfeREnCE
The $\bullet$ denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. (Note 3)

| SYMBOL | PARAMETER | CONDITIONS | MIN | TYP MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $1 \mathrm{IN}^{+}$ | Absolute/Common Mode IN+ Voltage |  | GND - 0.3V | $\mathrm{V}_{\text {CC }}+0.3 \mathrm{~V}$ | V |
| $\underline{1 N^{-}}$ | Absolute/Common Mode IN- Voltage |  | GND - 0.3V | $\mathrm{V}_{\text {CC }}+0.3 \mathrm{~V}$ | V |
| FS | Full-Scale of the Differential Input ( $\left.\mathrm{IN}^{+}-\mathrm{IN}^{-}\right)$ | $\bullet$ | $0.5 \mathrm{~V}_{\text {REF }}$ |  | V |
| LSB | Least Significant Bit of the Output Code | - | FS/2 ${ }^{24}$ |  |  |
| VIN | Input Differential Voltage Range ( $\mathrm{IN}^{+}$- $\mathrm{IN}^{-}$) | $\bullet$ | -FS | +FS | V |
| $\mathrm{V}_{\text {REF }}$ | Reference Voltage Range ( $\mathrm{REF}^{+}$- REF- ) | $\bullet$ | 0.1 | $V_{C C}$ | V |

 temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. (Note 3)

| SYMBOL | PARAMETER | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{C}_{\text {S }}(\mathrm{IN}+$ | IN+ Sampling Capacitance |  |  |  | 11 |  | pF |
| $\mathrm{C}_{S}\left(\mathrm{IN}^{-}\right)$ | IN- Sampling Capacitance |  |  |  | 11 |  | pF |
| $\mathrm{C}_{\text {S }}\left(\mathrm{V}_{\text {REF }}\right)$ | $V_{\text {REF }}$ Sampling Capacitance |  |  |  | 11 |  | pF |
| IDC_LEAK (IN+) | IN+ DC Leakage Current | Sleep Mode, $\mathrm{IN}^{+}$= GND | $\bullet$ | -10 | 1 | 10 | nA |
| IDC_LEAK (IN-) | IN ${ }^{-}$DC Leakage Current | Sleep Mode, $\mathrm{IN}^{-}=$GND | $\bullet$ | -10 | 1 | 10 | nA |
| $\underline{\text { IDC_LEAK ( } \mathrm{V}_{\text {REF }} \text { ) }}$ | REF+ ${ }^{+}$REF ${ }^{-}$DC Leakage Current | Sleep Mode, $\mathrm{V}_{\text {REF }}=\mathrm{V}_{\text {CC }}$ | $\bullet$ | -100 | 1 | 100 | nA |

## $I^{2}$ C DIGITAL IIPUTS ARD DIGITAL OUTPUTS <br> The - denotes the specifications which apply over

 the full operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. (Note 3)| SYMBOL | PARAMETER | CONDITIONS |  | MIN | TYP MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {IH }}$ | High Level Input Voltage |  | $\bullet$ | $0.7 \mathrm{~V}_{C C}$ |  | V |
| $\mathrm{V}_{\text {IL }}$ | Low Level Input Voltage |  | $\bullet$ |  | $0.3 \mathrm{~V}_{\text {CC }}$ | V |
| $\mathrm{V}_{\text {IL(CA1 }}$ | Low Level Input Voltage for Address Pin |  | $\bullet$ |  | $0.05 \mathrm{~V}_{\text {c }}$ | V |
| $\mathrm{V}_{\text {IH(CAO/f0, }{ }^{\text {ca1 }} \text { ) }}$ | High Level Input Voltage for Address Pins |  | $\bullet$ | $0.95 \mathrm{~V}_{\text {c }}$ |  | V |
| RINH | Resistance from CAO/fo, CA1 to $\mathrm{V}_{\text {CC }}$ to Set Chip Address Bit to 1 |  | $\bullet$ |  | 10 | k $\Omega$ |
| $\mathrm{R}_{\text {INL }}$ | Resistance from CA1 to GND to Set Chip Address Bit to 0 |  | $\bullet$ |  | 10 | k $\Omega$ |
| $\mathrm{R}_{\text {INF }}$ | Resistance from CA0/f ${ }_{0}$, CA1 to $\mathrm{V}_{\text {CC }}$ or GND to Set Chip Address Bit to Float |  | $\bullet$ | 2 |  | $\mathrm{M} \Omega$ |
| I | Digital Input Current |  | $\bullet$ | -10 | 10 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {HYS }}$ | Hysteresis of Schmitt Trigger Inputs | (Note 5) |  | $0.05 \mathrm{~V}_{C C}$ |  | V |
| $\mathrm{V}_{\text {OL }}$ | Low Level Output Voltage SDA | $\mathrm{I}=3 \mathrm{~mA}$ | $\bullet$ |  | 0.4 | V |
| $\mathrm{t}_{\mathrm{OF}}$ | Output Fall Time from $\mathrm{V}_{\text {IHMIN }}$ to $\mathrm{V}_{\text {ILMAX }}$ | Bus Load C ${ }_{\text {B }} 10 \mathrm{pF}$ to 400pF (Note 14) | $\bullet$ | $20+0.1 \mathrm{C}_{\mathrm{B}}$ | 250 | ns |
| tsp | Input Spike Suppression |  | $\bullet$ |  | 50 | ns |
| IN | Input Leakage | $0.1 V_{\text {CC }} \leq V_{\text {IN }} \leq V_{C C}$ | $\bullet$ |  | 1 | $\mu \mathrm{A}$ |
| $\mathrm{Cl}_{1}$ | Capacitance for Each I/O Pin |  | $\bullet$ | 10 |  | pF |
| $\mathrm{C}_{\mathrm{B}}$ | Capacitance Load for Each Bus Line |  | $\bullet$ |  | 400 | pF |
| $\mathrm{C}_{\text {CAX }}$ | External Capacitive Load On-Chip Address Pins (CAO/f ${ }_{0}$,CA1) for Valid Float |  | $\bullet$ |  | 10 | pF |
| $\mathrm{V}_{\text {IH(EXT,OSC) }}$ | High Level CAO/fo External Oscillator | $2.7 \mathrm{~V} \leq \mathrm{V}_{\text {CC }}<5.5 \mathrm{~V}$ | $\bullet$ | $\mathrm{V}_{\text {CC }}-0.5 \mathrm{~V}$ |  | V |
| $\mathrm{V}_{\text {IL(EXT,OSC) }}$ | Low Level CAO/f ${ }_{0}$ External Oscillator | $2.7 \mathrm{~V} \leq \mathrm{V}_{\text {CC }}<5.5 \mathrm{~V}$ | $\bullet$ |  | 0.5 | V |

POWER REQUIREMERTS
The o denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. (Note 3)

| SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
| :--- | :--- | :--- | :--- | :--- | :---: | :---: |
| $V_{\text {CC }}$ | Supply Voltage |  | $\bullet$ | 2.7 | 5.5 | V |
| $I_{\text {CC }}$ | Supply Current | Conversion Mode (Note 11) | $\bullet$ | 160 | 250 | $\mu \mathrm{~A}$ |
|  |  | Sleep Mode (Note 11) | $\bullet$ | 1 | 2 | $\mu \mathrm{~A}$ |

TIMING CHARACTERISTICS The $\bullet$ denotes the speciifications which apply vere the full operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. (Note 3)

| SYMBOL | PARAMETER | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{f}_{\text {EOSC }}$ | External Oscillator Frequency Range |  | $\bullet$ | 10 |  | 1000 | kHz |
| theo | External Oscillator High Period |  | $\bullet$ | 0.125 |  | 100 | $\mu \mathrm{S}$ |
| tLEO | External Oscillator Low Period |  | $\bullet$ | 0.125 |  | 100 | $\mu \mathrm{S}$ |
| tconv_1 | Conversion Time for 1x Speed Mode | 50Hz Mode <br> 60Hz Mode <br> Simultaneous 50Hz/60Hz Mode <br> External Oscillator (Note 10) | $\stackrel{\bullet}{\bullet}$ | $\begin{aligned} & 157.2 \\ & 131.0 \\ & 144.1 \end{aligned}$ | $\begin{gathered} 160.3 \\ 133.6 \\ 146.9 \\ 41036 / f_{\text {EOSC }} \\ \hline \end{gathered}$ | $\begin{aligned} & 163.5 \\ & 136.3 \\ & 149.9 \end{aligned}$ | ms ms ms ms |
| tconv_2 | Conversion Time for 2x Speed Mode | 50Hz Mode <br> 60Hz Mode <br> Simultaneous $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ Mode <br> External Oscillator (Note 10) | $\stackrel{\bullet}{\bullet}$ | $\begin{aligned} & 78.7 \\ & 65.6 \\ & 72.2 \end{aligned}$ | $\begin{gathered} 80.3 \\ 66.9 \\ 73.6 \\ \text { 20556/f } \\ \text { EOSC } \end{gathered}$ | $\begin{aligned} & 81.9 \\ & 68.2 \\ & 75.1 \end{aligned}$ | ms ms ms ms |

## $\mathbf{I}^{2} \mathrm{C}$ TIming Characteristics

The $\bullet$ denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. (Notes 3,15 )

| SYMBOL | PARAMETER | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{f}_{\text {SCL }}$ | SCL Clock Frequency |  | $\bullet$ | 0 |  | 400 | kHz |
| thD(SDA) | Hold Time (Repeated) START Condition |  | $\bullet$ | 0.6 |  |  | $\mu \mathrm{s}$ |
| tow | LOW Period of the SCL Clock Pin |  | $\bullet$ | 1.3 |  |  | $\mu \mathrm{S}$ |
| thigh | HIGH Period of the SCL Clock Pin |  | $\bullet$ | 0.6 |  |  | $\mu \mathrm{S}$ |
| $\mathrm{t}_{\text {SU(STA) }}$ | Set-Up Time for a Repeated START Condition |  | $\bullet$ | 0.6 |  |  | $\mu \mathrm{S}$ |
| ${ }^{\text {thD(DAT) }}$ | Data Hold Time |  | $\bullet$ | 0 |  | 0.9 | $\mu \mathrm{S}$ |
| $\left.\underline{t_{S U}(\mathrm{DAT}}\right)$ | Data Set-Up Time |  | $\bullet$ | 100 |  |  | ns |
| $\mathrm{tr}_{\underline{r}}$ | Rise Time for Both SDA and SCL Signals | (Note 14) | $\bullet$ | $20+0.1 C_{B}$ |  | 300 | ns |
| $\mathrm{t}_{\mathrm{f}}$ | Fall Time for Both SDA and SCL Signals | (Note 14) | $\bullet$ | $20+0.1 C_{B}$ |  | 300 | ns |
| $\mathrm{t}_{\text {SU(STO) }}$ | Set-Up Time for STOP Condition |  | $\bullet$ | 0.6 |  |  | $\mu \mathrm{S}$ |

Note 1: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.
Note 2: All voltage values are with respect to GND.
Note 3: $\mathrm{V}_{\mathrm{CC}}=2.7 \mathrm{~V}$ to 5.5 V unless otherwise specified.

$$
\begin{aligned}
& \mathrm{V}_{\text {REF }}=\text { REF }^{+}-\text {REF }^{-}, \mathrm{V}_{\text {REFCM }}=\left(\text { REF }^{+}+\mathrm{REF}^{-}\right) / 2, \mathrm{FS}=0.5 \mathrm{~V}_{\text {REF }} ; \\
& V_{\text {IN }}=I N^{+}-I N^{-}, V_{\text {INCM }}=\left(\mathrm{IN}^{+}+\mathrm{IN}^{-}\right) / 2 .
\end{aligned}
$$

Note 4: Use internal conversion clock or external conversion clock source with $\mathrm{f}_{\text {EOSC }}=307.2 \mathrm{kHz}$ unless otherwise specified.
Note 5: Guaranteed by design, not subject to test.
Note 6: Integral nonlinearity is defined as the deviation of a code from a straight line passing through the actual endpoints of the transfer curve. The deviation is measured from the center of the quantization band.

Note 7: 50 Hz mode (internal oscillator) or $\mathrm{f}_{\mathrm{EOSC}}=256 \mathrm{kHz} \pm 2 \%$ (external oscillator).
Note 8: 60 Hz mode (internal oscillator) or $\mathrm{f}_{\mathrm{EOSC}}=307.2 \mathrm{kHz} \pm 2 \%$ (external oscillator).
Note 9: Simultaneous $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ mode (internal oscillator) or $\mathrm{f}_{\mathrm{EOSC}}=$ $280 \mathrm{kHz} \pm 2 \%$ (external oscillator).
Note 10: The external oscillator is connected to the $\mathrm{CAO}_{\mathrm{f}}^{0} 0 \mathrm{pin}$. The external oscillator frequency, $\mathrm{f}_{\mathrm{EOSC}}$, is expressed in kHz .
Note 11: The converter uses the internal oscillator.
Note 12: The output noise includes the contribution of the internal calibration operations.
Note 13: Guaranteed by design and test correlation.
Note 14: $C_{B}=$ capacitance of one bus line in pF .
Note 15: All values refer to $\mathrm{V}_{I H(M I N)}$ and $\mathrm{V}_{\mathrm{IL}(\mathrm{MAX})}$ levels.

## TYPICAL PERFORMANCE CHARACTERISTICS



2485 G01


2485 G04

Integral Nonlinearity
$\left(V_{C C}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{REF}}=2.5 \mathrm{~V}\right)$


2485 G02

Total Unadjusted Error
$\left(V_{C C}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{REF}}=2.5 \mathrm{~V}\right)$


2485 G05

Noise Histogram (7.5sps)


Integral Nonlinearity
$\left(V_{C C}=2.7 \mathrm{~V}, \mathrm{~V}_{\text {REF }}=2.5 \mathrm{~V}\right)$


2485 G03

Total Unadjusted Error
( $\mathrm{V}_{\text {CC }}=2.7 \mathrm{~V}, \mathrm{~V}_{\text {REF }}=2.5 \mathrm{~V}$ )


2485 G06


## TYPICAL PERFORMANCE CHARACTERISTICS




RMS Noise vs Temperature ( $\mathrm{T}_{\mathrm{A}}$ )





2485 G13



## LTC2485

## TYPICAL PERFORMANCE CHARACTERISTICS



2485 G 19


2485 G22

## Sleep Mode Current vs Temperature




PSRR vs Frequency at $V_{c c}$


2485 G23
Conversion Current
vs Output Data Rate


PSRR vs Frequency at $V_{\text {CC }}$


Conversion Current vs Temperature


Integral Nonlinearity (2x Speed Mode; $\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{\text {REF }}=5 \mathrm{~V}$ )


TYPICAL PERFORMANCE CHARACTERISTICS


2485 G28


2485 G31

(2x Speed Mode)

Integral Nonlinearity ( $2 x$ Speed
Mode; $\mathrm{V}_{\text {CC }}=2.7 \mathrm{~V}$, $\mathrm{V}_{\text {REF }}=2.5 \mathrm{~V}$ )


2485 G29

Offset Error vs VIN(CM)
(2x Speed Mode)


## Offset Error vs VREF

(2x Speed Mode)


Noise Histogram
(2x Speed Mode)


Offset Error vs Temperature
(2x Speed Mode)


PSRR vs Frequency at $V_{\text {CC }}$ (2x Speed Mode)


## TYPICAL PERFORMANCE CHARACTERISTICS



2485 G37

PSRR vs Frequency at $V_{\text {CC }}$
(2x Speed Mode)


## PIn fUnCTIOnS

REF ${ }^{+}$(Pin 1), REF- (Pin 3): Differential Reference Input. The voltage on these pins can have any value between GND and $V_{C C}$ as long as the reference positive input, REF $^{+}$, is more positive than the reference negative input, REF ${ }^{-}$, by at least 0.1 V .

VCC (Pin 2): Positive Supply Voltage. Bypass to GND (Pin 8) with a $1 \mu \mathrm{~F}$ tantalum capacitor in parallel with $0.1 \mu \mathrm{~F}$ ceramic capacitor as close to the part as possible.
$\mathbf{I N}^{+}$(Pin 4), $\mathbf{I N}^{-}$(Pin 5): Differential Analog Input. The voltage on these pins can have any value between GND -0.3V and $\mathrm{V}_{\mathrm{CC}}+0.3 \mathrm{~V}$. Within these limits the converter bipolar input range $\left(\mathrm{V}_{\mathrm{IN}}=\mathrm{IN}^{+}-\mathrm{IN}^{-}\right)$extends from $-0.5 \bullet \mathrm{~V}_{\text {REF }}$ to $0.5 \cdot V_{\text {REF }}$. Outside this input range the converter produces unique overrange and underrange output codes.
SCL (Pin 6): Serial Clock Pin of the $I^{2} \mathrm{C}$ Interface. The LTC2485 can only act as a slave and the SCL pin only accepts external serial clock. Data is shifted into the SDA pin on the rising edges of the SCL clock and output through the SDA pin on the falling edges of the SCL clock.

SDA (Pin 7): Bidirectional Serial Data Line of the $I^{2} \mathrm{C}$ Interface. In the transmitter mode (Read), the conversion result is output through the SDA pin, while in the receiver mode (Write), the device configuration bits are input through the SDA pin. At data input mode, the pin is high impedance; while at data output mode, it is an open-drain N -channel driver and therefore an external pull-up resistor or current source to $V_{C C}$ is needed.

GND (Pin 8): Ground. Connect this pin to a ground plane through a low impedance connection.
CA1 (Pin 9): Chip Address Control Pin. The CA1 pin is configured as a three state (LOW, HIGH, or Floating) address control bit for the device $\mathrm{I}^{2} \mathrm{C}$ address.

CAO/fo (Pin 10): Chip Address Control Pin/External Clock Input Pin. When no transition is detected on the $\mathrm{CAO} / \mathrm{f}_{0}$ pin, it is a two state (HIGH or Floating) address control bit for the device $\mathrm{I}^{2} \mathrm{C}$ address. When the pin is driven by an external clock signal with a frequency $\mathrm{f}_{\mathrm{EOSC}}$ of at least 10 kHz , the converter uses this signal as its system clock and the fundamental digital filter rejection null is located at a frequency $\mathrm{f}_{\mathrm{EOSC}} / 5120$ and sets the Chip Address CAO internally to a HIGH.

## functional block pingram



## APPLICATIONS INFORMATION

## CONVERTER OPERATION

## Converter Operation Cycle

The LTC2485 is alow power, $\Delta \Sigma$ analog-to-digital converter with an $I^{2} \mathrm{C}$ interface. After power on reset, its operation is made up of three states. The converter operating cycle begins with the conversion, followed by the low power sleep state and ends with the data output/input (see Figure 1).


Figure 1. LTC2485 State Transition Diagram
Initially, the LTC2485 performs a conversion. Once the conversion is complete, the device enters the sleep state. While in this sleep state, power consumption is reduced by two orders of magnitude. The part remains in the sleep state as long as it is not addressed for a read/write operation. The conversion result is held indefinitely in a static shift register while the converter is in the sleep state.

The device will not acknowledge an external request during the conversion state. After a conversion is finished,
the device is ready to accept a read/write request. Once the LTC2485 is addressed for a read operation, the device begins outputting the conversion result under control of the serial clock (SCL). There is no latency in the conversion result. The data output is 32 bits long and contains a 24-bit plus sign conversion result. This result is shifted out on the SDA pin under the control of the SCL. Data is updated on the falling edges of SCL allowing the user to reliably latch data on the rising edge of SCL. In write operation, the device accepts one configuration byte and the data is shifted in on the rising edges of the SCL. A new conversion is initiated by a STOP condition following a valid write operation or at the conclusion of a data read operation (read out all 32 bits).

## $I^{2} \mathrm{C}$ INTERFACE

The LTC2485 communicates through an $I^{2} C$ interface. The $I^{2} C$ interface is a 2 -wire open-drain interface supporting multiple devices and masters on a single bus. The connected devices can only pull the bus wires LOW and they never drive the bus HIGH. The bus wires are externally connected to a positive supply voltage via a current-source or pull-up resistor. When the bus is free, both lines are HIGH. Data on the ${ }^{2} \mathrm{C}$-bus can be transferred at rates of up to $100 \mathrm{kbit} / \mathrm{s}$ in the Standard-mode and up to 400kbit/s in the Fast-mode. The V $\mathrm{VCC}^{\text {power should not }}$ be removed from the device when the $I^{2} \mathrm{C}$ bus is active to avoid loading the $I^{2} \mathrm{C}$ bus lines through the internal ESD protection diodes.
Each device on the $I^{2} \mathrm{C}$ bus is recognized by a unique address stored in that device and can operate as either a transmitter or receiver, depending on the function of the device. In addition to transmitters and receivers, devices can also be considered as masters or slaves when performing data transfers. A master is the device which initiates a data transfer on the bus and generates the clock signals to permit that transfer. At the same time any device addressed is considered a slave.

The LTC2485 can only be addressed as a slave. Once addressed, it can receive configuration bits or transmit the last conversion result. Therefore the serial clock line SCL

## APPLICATIONS InFORMATION

is an input only and the data line SDA is bidirectional. The device supports the Standard-mode and the Fast-mode for data transfer speeds up to 400kbit/s. Figure 2 shows the definition of timing for Fast/Standard-mode devices on the $\mathrm{I}^{2} \mathrm{C}$-bus.

## The START and STOP Conditions

A START condition is generated by transitioning SDA from HIGH to LOW while SCL is HIGH. The bus is considered to be busy after the START condition. When the data transfer is finished, a STOP condition is generated by transitioning SDA from LOW to HIGH while SCL is HIGH. The bus is free again a certain time after the STOP condition. START and STOP conditions are always generated by the master.

When the bus is in use, it stays busy if a repeated START $(\mathrm{Sr})$ is generated instead of a STOP condition. The repeated START (Sr) conditions are functionally identical to the START (S).

## Data Transferring

After the START condition, the $I^{2} \mathrm{C}$ bus is busy and data transfer is set between a master and a slave. Data is transferred over $I^{2} \mathrm{C}$ in groups of nine bits (one byte) followed by an acknowledge bit, therefore each group takes nine SCL cycles. The transmitter releases the SDA line during the acknowledge clock pulse and the receiver issues an Acknowledge (ACK) by pulling SDA LOW or leaves SDA HIGH to indicate a Not Acknowledge (NAK) condition. Change of data state can only happen while SCL is LOW.

## Accessing the Special Features of the LTC2485

The LTC2485 combines a high resolution, low noise $\Delta \Sigma$ analog-to-digital converter with an on-chip selectable temperature sensor, programmable digital filter and output rate control. These special features are selected through a single 8-bit serial input word during the data input/output cycle (see Figure 3).


2485 F02
Figure 2. Definition of Timing for $\mathrm{F} / \mathrm{S}$-Mode Devices on the $\mathrm{I}^{2} \mathrm{C}$-Bus


Figure 3. Timing Diagram for Writing to the LTC2485

## APPLICATIONS InFORMATION

The LTC2485 powers up in a default mode commonly used for most measurements. The device will remain in this mode until a valid write cycle is performed. In this default mode, the measured input is external, the digital filter simultaneously rejects 50 Hz and 60 Hz line frequency noise, and the speed mode is $1 x$ (offset automatically, continuously calibrated).
The $I^{2} \mathrm{C}$ serial interface grants access to any or all special functions contained withinthe LTC2485. In orderto change the mode of operation, a valid write address followed by 8 bits of data are shifted into the device (see Table 1). The first 4 bits are reserved and should be low. The 5th bit (IM) is used to select the internal temperature sensor as the conversion input, while the 6th and 7th bits (FA, FB) combine to determine the line frequency rejection mode. The 8th bit (SPD) is used to double the output rate by disabling the offset auto calibration.

Table 1. Selecting Special Modes

| IM | FA | FB | SPD | COMMENTS |
| :---: | :---: | :---: | :---: | :--- |
| 0 | 0 | 0 | 0 | External Input, 50 Hz and 60 Hz Rejection, <br> Auto-Calibration |
| 0 | 0 | 1 | 0 | External Input, 50 Hz Rejection, <br> Auto-Calibration |
| 0 | 1 | 0 | 0 | External Input, 60 Hz Rejection, <br> Auto-Calibration |
| 0 | 0 | 0 | 1 | External Input, 50 Hz and 60 Hz Rejection, <br> $2 x$ Speed |
| 0 | 0 | 1 | 1 | External Input, 50 Hz Rejection, $2 x$ Speed |
| 0 | 1 | 0 | 1 | External Input, 60 Hz Rejection, $2 x$ Speed |
| 1 | 0 | 0 | 0 | Temperature Input, 50 Hz and 60 Hz <br> Rejection, Auto-Calibration |
| 1 | 0 | 1 | X | Temperature Input, 50 Hz Rejection, <br> Auto-Calibration |
| 1 | 1 | 0 | X | Temperature Input, 60 Hz Rejection, <br> Auto-Calibration |
| X | 1 | 1 | X | Reserved, Do Not Use |

## Temperature Sensor (IM)

The LTC2485 includes an on-chip temperature sensor. The temperature sensor is selected by setting $\mathrm{IM}=1$ in the serial input data stream. Conversions are performed directly on the temperature sensor by the converter. While operating in this mode, the device behaves as a temperature to bits converter. The digital reading is proportional to the absolute temperature of the device. This feature allows the converter to linearize temperature sensors or continuously remove temperature effects from external sensors. Several applications leveraging this feature are presented in more detail in the applications section. While operating in this mode, the speed is set to normal independent of the control bit (SPD).

## Rejection Mode (FA, FB)

The LTC2485 includes a high accuracy on-chip oscillator with no required external components. Coupled with a 4th order digital lowpass filter, the LTC2485 rejects line frequency noise. In the default mode, the LTC2485 simultaneously rejects 50 Hz and 60 Hz by at least 87 dB . The LTC2485 can also be configured to selectively reject 50 Hz or 60 Hz to better than 110 dB .

## Speed Mode (SPD)

The LTC2485 continuously performs offset calibrations. Every conversion cycle, two conversions are automatically performed (default) and the results combined. This result is free from offset and drift. In applications where the offset is not critical, the auto-calibration feature can be disabled with the benefit of twice the output rate.

Linearity, full-scale accuracy and full-scale drift are identical for both $2 x$ and $1 x$ speed modes. In both the $1 x$ and $2 x$ speed there is no latency. This enables input steps or multiplexer channel changes to settle in a single conversion cycle easing system overhead and increasing the effective conversion rate.

## APPLICATIONS InFORMATION

## LTC2485 Data Format

After a START condition, the master sends a 7-bit address followed by a R/W bit. The bit R/W is 1 for a Read request and 0 for a Write request. If the 7-bit address agrees with an LTC2485's address, that device is selected. When the device is in the conversion state, it does not accept the request and issues a Not-Acknowledge (NAK) by leaving SDA HIGH. A write operation will also generate an NAK signal. If the conversion is complete, it issues an acknowledge (ACK) by pulling SDA LOW.

The LTC2485 has two registers. The output register contains the result of the last conversion and a user programmable configuration register that sets the converter operation mode.

The output register contains the last conversion result. After each conversion is completed, the device automatically enters the sleep state where the supply current is reduced to $1 \mu \mathrm{~A}$. When the LTC2485 is addressed for a Read operation, it acknowledges (by pulling SDA LOW) and acts as a transmitter. The master and receiver can read up to four bytes from the LTC2485. After a complete Read operation (4 bytes), the output register is emptied, a new conversion is initiated, and a following Read request in the same output phase will be NAKed. The LTC2485 output data stream is 32 bits long, shifted out on the falling edges of SCL. The first bit is the conversion result sign bit (SIG), (see Tables 2 and 3). This bit is HIGH if $\mathrm{V}_{\mathrm{IN}} \geq 0$.

It is LOW if $\mathrm{V}_{\text {IN }}<0$. The second bit is the most significant bit (MSB) of the result. The first two bits (SIG and MSB) can be used to indicate over range conditions. If both bits are HIGH , the differential input voltage is above +FS and the following 24 bits are set to LOW to indicate an overrange condition. If both bits are LOW, the input voltage is below -FS and the following 24 bits are set to HIGH to indicate an underrange condition. The function of these two bits is summarized in Table 1. The next 24 bits contain the conversion results in binary two's complement format. The remaining six bits are Sub LSBs below the 24-bit level.

As long as the voltage on the $\mathrm{IN}^{+}$and $\mathrm{IN}^{-}$pins is maintained within the -0.3 V to $\left(\mathrm{V}_{c \mathrm{C}}+0.3 \mathrm{~V}\right)$ absolute maximum operating range, a conversion result is generated for any differential input voltage $\mathrm{V}_{\text {IN }}$ from $-\mathrm{FS}=-0.5 \bullet \mathrm{~V}_{\text {REF }}$ to + FS=0.5 • V REF. For differential input voltages greater than +FS , the conversion result is clamped to the value corresponding to the + FS +1 LSB. For differential input voltages below -FS, the conversion result is clamped to the value corresponding to -FS - 1LSB.

Table 2. LTC2485 Status Bits

| INPUT RANGE | BIT 31 SIG | BIT 30 MSB |
| :--- | :---: | :---: |
| $V_{\text {IN }} \geq 0.5 \cdot V_{\text {REF }}$ | 1 | 1 |
| $O V^{\leq} V_{\text {IN }}<0.5 \cdot V_{\text {REF }}$ | $1 / 0$ | 0 |
| $-0.5 \cdot V_{\text {REF }} \leq V_{\text {IN }}<0 \mathrm{~V}$ | 0 | 1 |
| $V_{\text {IN }}<-0.5 \cdot V_{\text {REF }}$ | 0 | 0 |

Table 3. LTC2485 Output Data Format

| DIFFERENTIAL INPUT VOLTAGE $\mathrm{V}_{\text {IN }}{ }^{*}$ | BIT 31 SIG | BIT 30 MSB | BIT 29 | BIT 28 | BIT 27 | ... | BIT 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{VIN}^{*} \geq \mathrm{FS}^{* *}$ | 1 | 1 | 0 | 0 | 0 | $\ldots$ | 0 |
| FS** - 1LSB | 1 | 0 | 1 | 1 | 1 | $\ldots$ | 1 |
| 0.5 • FS** | 1 | 0 | 1 | 0 | 0 | $\ldots$ | 0 |
| $0.5 \cdot \mathrm{FS}^{* *}$ - 1LSB | 1 | 0 | 0 | 1 | 1 | ... | 1 |
| 0 | 1/0*** | 0 | 0 | 0 | 0 | $\ldots$ | 0 |
| -1LSB | 0 | 1 | 1 | 1 | 1 | ... | 1 |
| -0.5 • FS** | 0 | 1 | 1 | 0 | 0 | $\ldots$ | 0 |
| -0.5 •FS** -1 LSB | 0 | 1 | 0 | 1 | 1 | ... | 1 |
| -FS** | 0 | 1 | 0 | 0 | 0 | $\ldots$ | 0 |
| $\mathrm{V}_{\text {IN }}{ }^{*}<-\mathrm{FS}^{* *}$ | 0 | 0 | 1 | 1 | 1 | ... | **** |

* The differential input voltage $\mathrm{V}_{\mathrm{IN}}=\mathrm{IN}^{+}-\mathrm{IN}^{-}$.
** The full-scale voltage FS $=0.5 \bullet V_{\text {ROF }}$.
*** The sign bit changes state during the 0 output code when the device is operating in the $2 x$ speed mode.
**** When operating in the $2 x$ speed mode, the underrange output is 0x3FFFxxx.


## APPLICATIONS InFORMATION

## Initiating a New Conversion

When the LTC2485 finishes a conversion, it automatically enters the sleep state. Once in the sleep state, the device is ready for a Read operation. After the device acknowledges a Read request, the device exits the sleep state and enters the data output state. The data output state concludes and the LTC2485 starts a new conversion once a STOP condition is issued by the master or all 32 bits of data are read out of the device.

During the data read cycle, a stop command may be issued by the master controller in order to start a new conversion and abort the data transfer. This stop command must be issued during the ninth clock cycle of a byte read when the bus is free (the ACK/NAK cycle).

## LTC2485 Address

The LTC2485 has two address pins, enabling one in 6 possible addresses, as shown in Table 4.

Table 4. LTC2485 Address Assignment

| CA1 | CAO/f $\mathbf{f}_{0}{ }^{*}$ | ADDRESS |
| :---: | :---: | :---: |
| LOW | HIGH | 0010100 |
| LOW | Floating | 0010101 |
| Floating | HIGH | 0010111 |
| Floating | Floating | 0100100 |
| HIGH | HIGH | 0100110 |
| HIGH | Floating | 0100111 |

* CAO/ $\mathrm{f}_{0}$ is treated as HIGH when driven by a valid external clock.

In addition to the configurable addresses listed in Table 4, the LTC2485 also contains a global address (1110111) which may be used for synchronizing multiple LTC2485s.


Figure 4. Timing Diagram for Reading from the LTC2485

APPLICATIONS INFORMATION

## OPERATION SEQUENCE

The LTC2485 acts as a transmitter or receiver. The device may be programmed to perform several functions. These include measuring an external differential input signal or an integrated temperature sensor, selecting line frequency rejection $(50 \mathrm{~Hz}, 60 \mathrm{~Hz}$, or simultaneous 50 Hz and 60 Hz$)$, and a $2 x$ speed up mode.

## Continuous Read

In applications where the configuration does not need to change for each conversion cycle, the conversion result can be continuously read. The configuration remains unchanged from the last value written into the device. If the device has not been written to since power up, the configuration is set to the default value (Input External, simultaneous $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ rejection, and $1 x$ speed mode). The operation sequence is shown in Figure 6. When the conversion is finished, the device may be addressed for
a read operation. At the end of a read operation, a new conversion begins. At the conclusion of the conversion cycle, the next result may be read using the method described above. If the conversion cycle is not concluded and a valid address selects the device, the LTC2485 generates a NAK signal indicating the conversion cycle is in progress.

## Continuous Read/Write

Once the conversion cycle is concluded, the LTC2485 can be written to then read from, using the repeated Start (Sr) command.

Figure 7 shows a cycle which begins with a data Write, a repeated start, followed by a read, and concluded with a stop command. The following conversion begins after all 32 bits are read out of the device or after the STOP command and uses the newly programmed configuration data.


Figure 5. The LTC2485 Conversion Sequence


Figure 6. Consecutive Reading at the Same Configuration


Figure 7. Write, Read, Start Conversion

## APPLICATIONS InFORMATION

## Discarding a Conversion Result and Initiating a New Conversion with Optional Configuration Updating

At the conclusion of a conversion cycle, a Write cycle can be initiated. Once the Write cycle is acknowledged, a stop $(P)$ command initiates a new conversion. If a new configuration is required, this data can be written into the device and a stop command initiates a new conversion, see Figure 8.

## Synchronizing Multiple LTC2485s with the Global Address Call

In applications where several LTC2485s are used on the same $I^{2} \mathrm{C}$ bus, all LTC2485s can be synchronized with the global address call. To achieve this, first all the LTC2485s must have completed the conversion cycle. The master issues a Start, followed by the LTC2485 global address 1110111 and a Write request. All LTC2485s will be selected and acknowledge the request. The master then sends the write byte (Optional) and ends the Write operation with a STOP. This will update the configuration registers (if a write byte was sent) and initiate a new conversion simultaneously on all the LTC2485s, as shown in Figure 9. In order to synchronize the start of conversion without affecting the configuration registers, the Write operation can be aborted with a STOP. This initiates a new conversion
on all the LTC2485s without changing the configuration registers.

## Easy Drive Input Current Cancellation

The LTC2485 combines a high precision delta-sigma ADC with an automatic differential input current cancellation front end. A proprietary front-end passive sampling network transparently removes the differential input current. This enables external RC networks and high impedance sensors to directly interface to the LTC2485 without external amplifiers. The remaining common mode input current is eliminated by either balancing the differential input impedances or setting the common mode input equal to the common mode reference (see Automatic Input Current Cancellation section). This unique architecture does not require on-chip buffers enabling input signals to swing all the way to ground and up to $\mathrm{V}_{\mathrm{Cc}}$. Furthermore, the cancellation does not interfere with the transparent offset and full-scale auto-calibration and the absolute accuracy (full-scale + offset + linearity) is maintained even with external RC networks.

## Conversion Clock

A major advantage the delta-sigma converter offers over conventional type converters is an on-chip digital filter


Figure 8. Start a New Conversion without Reading Old Conversion Result


Figure 9. Synchronize the LTC2485s with the Global Address Call

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(commonly implemented as a SINC or Comb filter). For high resolution, low frequency applications, this filter is typically designed to reject line frequencies of 50 Hz or 60 Hz plus their harmonics. The filter rejection performance is directly related to the accuracy of the converter system clock. The LTC2485 incorporates a highly accurate on-chip oscillator. This eliminates the need for external frequency setting components such as crystals or oscillators.

## Frequency Rejection Selection (CAO/fo)

The LTC2485 internal oscillator provides better than 110dB normal mode rejection at the line frequency and all its harmonics (up to the 255 th) for $50 \mathrm{~Hz} \pm 2 \%$ or $60 \mathrm{~Hz} \pm 2 \%$, or better than 87 dB normal mode rejection from 48 Hz to 62.4 Hz . The rejection mode is selected by writing to the on-chip configuration register (the default mode at powerup is simultaneous $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ rejection).
When a fundamental rejection frequency different from 50 Hz or 60 Hz is required or when the converter must be synchronized with an outside source, the LTC2485 can operate with an external conversion clock. The converter automatically detects the presence of an external clock signal at the $\mathrm{CAO} / \mathrm{f}_{0}$ pin and turns off the internal oscillator. The chip address for CAO is internally set HIGH. The frequency $\mathrm{f}_{\text {EOSC }}$ of the external signal must be at least 10 kHz to be detected. The external clock signal duty cycle is not significant as long as the minimum and maximum specifications for the high and low periods theo and tLEO are observed.

While operating with an external conversion clock of a frequency ${ }_{\text {EOSC }}$, the LTC2485 provides better than 110dB normal mode rejection in a frequency range of $f_{E O S S} / 5120$
$\pm 4 \%$ and its harmonics. The normal mode rejection as a function of the input frequency deviation from $\mathrm{f}_{\mathrm{EOSC}} / 5120$ is shown in Figure 10.


Figure 10. LTC2485 Normal Mode Rejection When Using an External Oscillator

Whenever an external clock is not present at the $\mathrm{CAO} / \mathrm{f}_{0}$ pin, the converter automatically activates its internal oscillator and enters the Internal Conversion Clock mode. CAO/fo may be tied HIGH or left floating in order to set the chip address. The LTC2485 operation will not be disturbed if the change of conversion clock source occurs during the sleep state or during the data output state while the converter uses an external serial clock. If the change occurs during the conversion state, the result of the conversion in progress may be outside specifications but the following conversions will not be affected.

Table 5 summarizes the duration of the conversion state of each state and the achievable output data rate as a function of $\mathrm{f}_{\mathrm{EOSC}}$.

Table 5. LTC2485 State Duration

| STATE | OPERATING MODE |  | DURATION |
| :---: | :---: | :---: | :---: |
| Conversion | Internal Oscillator | 60Hz Rejection | 133ms, Output Data Rate $\leq 7.5$ Readings/s for 1x Speed Mode 67 ms , Output Data Rate $\leq 15$ Readings/s for $2 x$ Speed Mode |
|  |  | 50Hz Rejection | 160 ms , Output Data Rate $\leq 6.2$ Readings/s for $1 \times$ Speed Mode 80ms, Output Data Rate $\leq 12.5$ Readings/s for $2 x$ Speed Mode |
|  |  | 50Hz/60Hz Rejection | 147 ms , Output Data Rate $\leq 6.8$ Readings/s for 1 x Speed Mode 73.6 ms , Output Data Rate $\leq 13.6$ Readings/s for $2 x$ Speed Mode |
|  | External Oscillator | CAO/f $\mathrm{f}_{0}=$ External Oscillator with Frequency $\mathrm{f}_{\mathrm{EOSC}} \mathrm{Hz}$ (f${ }_{\mathrm{EOSC}} / 5120$ Rejection) | 41036/f EOSCS , Output Data Rate $\leq f_{\text {EOSC }} / 41036$ Readings/s for 1x Speed Mode 20556/f EOSCS , Output Data Rate $\leq \mathrm{f}_{\text {EOSC }} / 20556$ Readings/s for 2x Speed Mode |

## APPLICATIONS InFORMATION

## Ease of Use

The LTC2485 data output has no latency, filter settling delay or redundant data associated with the conversion cycle. There is a one-to-one correspondence between the conversion and the output data. Therefore, multiplexing multiple analog voltages is easy.
The LTC2485 performs offset and full-scale calibrations every conversion cycle. This calibration is transparent to the user and has no effect on the cyclic operation described above. The advantage of continuous calibration is extreme stability of offset and full-scale readings with respect to time, supply voltage change and temperature drift.

## Power-Up Sequence

The LTC2485 automatically enters an internal reset state when the power supply voltage $V_{C C}$ drops below approximately 2 V . This feature guarantees the integrity of the conversion result.

When the $\mathrm{V}_{\text {CC }}$ voltage rises above this critical threshold, the converter creates an internal power-on-reset (POR) signal with a duration of approximately 4ms. The POR signal clears all internal registers. Following the POR signal, the LTC2485 starts a normal conversion cycle and follows the succession of states described in Figure 1. The first conversion result following POR is accurate within the specifications of the device if the power supply voltage is restored within the operating range ( 2.7 V to 5.5 V ) before the end of the POR time interval.

## On-Chip Temperature Sensor

The LTC2485 contains an on-chip PTAT (proportional to absolute temperature) signal that can be used as a temperature sensor. The internal PTAT has a typical value of 420 mV at $27^{\circ} \mathrm{C}$ and is proportional to the absolute temperature value with a temperature coefficient of 420/(27 + 273) = $1.40 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ (SLOPE), as shown in Figure 11. The internal PTAT signal is used in a single-ended mode referenced to device ground internally. The 1x speed mode with automatic offset calibration is automatically selected for the internal PTAT signal measurement as well.

When using the internal temperature sensor, if the output code is normalized to $\mathrm{R}_{\mathrm{SDA}}=\mathrm{V}_{\mathrm{PTAT}} / V_{\text {REF }}$, the temperature is calculated using the following formula:

$$
T_{K}=\frac{R_{\text {SDA }} \cdot V_{\text {REF }}}{\text { SLOPE }} \text { in Kelvin }
$$

and

$$
\mathrm{T}_{\mathrm{C}}=\frac{\mathrm{R}_{\mathrm{SDA}} \cdot \mathrm{~V}_{\text {REF }}}{\mathrm{SLOPE}}-273 \text { in }^{\circ} \mathrm{C}
$$

where SLOPE is nominally $1.4 \mathrm{mV} /{ }^{\circ} \mathrm{C}$.
Since the PTAT signal can have an initial value variation which results in errors in SLOPE, to achieve absolute temperature measurements, a one-time calibration is needed to adjust the SLOPE value. The converter output of the PTAT signal, $R 0_{\text {SDA }}$, is measured at a known temperature TO (in ${ }^{\circ} \mathrm{C}$ ) and the SLOPE is calculated as:

$$
\text { SLOPE }=\frac{R 0_{\text {SDA }} \bullet V_{\text {REF }}}{\mathrm{T} 0+273}
$$

This calibrated SLOPE can be used to calculate the temperature.
If the same $V_{\text {REF }}$ source is used during calibration and temperature measurement, the actual value of the $\mathrm{V}_{\text {REF }}$ is not needed to measure the temperature as shown in the calculation below:

$$
\begin{aligned}
T_{C} & =\frac{R_{\text {SDA }} \cdot V_{\text {REF }}}{S L O P E}-273 \\
& =\frac{R_{\text {SDA }}}{R 0_{\text {SDA }}} \cdot(T 0+273)-273
\end{aligned}
$$



Figure 11. Internal PTAT Signal vs Temperature

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## Reference Voltage Range

The LTC2485 external reference voltage range is 0.1 V to $\mathrm{V}_{\mathrm{CC}}$. The converter output noise is determined by the thermal noise of the front-end circuits, and as such, its value in nanovolts is nearly constant with reference voltage. A reduced reference voltage will improve the converter performance when operated with an external conversion clock (external $\mathrm{f}_{0}$ signal) at substantially higher output data rates (see the Output Data Rate section). V REF must be $\geq 1.1 \mathrm{~V}$ to use the internal temperature sensor.
The reference input is differential. The differential reference input range ( $V_{\text {REF }}=$ REF $^{+}-$REF $^{-}$) is 100 mV to $V_{C C}$ and the common mode reference input range is 0 V to $\mathrm{V}_{\mathrm{CC}}$.

## Input Voltage Range

The analog input is truly differential with an absolute/ common mode range for the $\mathrm{IN}^{+}$and $\mathrm{IN}^{-}$input pins extending from GND -0.3 V to $\mathrm{V}_{\mathrm{CC}}+0.3 \mathrm{~V}$. Outside these limits, the ESD protection devices begin to turn on and the errors due to input leakage current increase rapidly. Within these limits, the LTC2485 converts the bipolar differential input signal, $\mathrm{V}_{\mathrm{IN}}=I \mathrm{~N}^{+}-\mathrm{IN}^{-}$, from -FS to +FS where $F S=0.5 \bullet V_{\text {REF }}$. Beyond this range, the converter indicates the overrange or the underrange condition using
distinct output codes. Since the differential input current cancellation does not rely on an on-chip buffer, current cancellation and DC performance is maintained rail-to-rail.

Input signals applied to $\mathrm{IN}^{+}$and $\mathrm{IN}^{-}$pins may extend by 300 mV below ground and above $\mathrm{V}_{\mathrm{CC}}$. In order to limit any fault current, resistors of up to 5 k may be added in series with the $\mathrm{IN}^{+}$and $\operatorname{IN}{ }^{-}$pins without affecting the performance of the devices. The effect of the series resistance on the converter accuracy can be evaluated from the curves presented inthe InputCurrent/ReferenceCurrent sections. In addition, series resistors will introduce a temperature dependent offset error due to the input leakage current. A 1nA input leakage current will develop a 1ppm offset error on a 5 k resistor if $\mathrm{V}_{\text {REF }}=5 \mathrm{~V}$. This error has a very strong temperature dependency.

## Driving the Input and Reference

The input and reference pins of the LTC2485 converter are directly connected to a network of sampling capacitors. Depending upon the relation between the differential input voltage and the differential reference voltage, these capacitors are switching between these four pins transferring small amounts of charge in the process. A simplified equivalent circuit is shown in Figure 12.


$$
\begin{aligned}
& I\left(\mathrm{IN}^{+}\right)_{\mathrm{AVG}}=I\left(\mathrm{IN}^{-}\right)_{\mathrm{AVG}}=\frac{\mathrm{V}_{\mathrm{IN}(\mathrm{CM})}-\mathrm{V}_{\mathrm{REF}(\mathrm{CM})}}{0.5 \bullet \mathrm{R}_{\mathrm{EQ}}}
\end{aligned}
$$

> where:
> $V_{\text {REFCM }}=\left(\frac{\mathrm{REF}^{+}+\mathrm{REF}^{-}}{2}\right), V_{\text {REF }}=\mathrm{REF}^{+}-\mathrm{REF}^{-}$
> $\mathrm{V}_{\mathrm{IN}}=\mathrm{IN}^{+}-\mathrm{IN}^{-}$
> $V_{\text {INCM }}=\left(\frac{\mathrm{IN}^{+}+\mathrm{IN}^{-}}{2}\right)$
> $\mathrm{R}_{\mathrm{EQ}}=2.71 \mathrm{M} \Omega$ INTERNAL OSCILLATOR 60 Hz MODE
> $\mathrm{R}_{\mathrm{EQ}}=2.98 \mathrm{M} \Omega$ INTERNAL OSCILLATOR 50 Hz AND 60 Hz MODE
> $\mathrm{R}_{\mathrm{EQ}}=\left(0.833 \bullet 10^{12}\right) / \mathrm{f}_{\mathrm{EOSC}}$ EXTERNAL OSCILLATOR
> $D_{T}$ IS THE DENSITY OF A DIGITAL TRANSITION AT THE MODULATOR OUTPUT
> WHERE REF ${ }^{-}$IS INTERNALLY TIED TO GND

SWITCHING FREQUENCY
$\mathrm{f}_{\mathrm{S}} \mathrm{w}=123 \mathrm{kHz}$ INTERNAL OSCILLATOR
$\mathrm{f}_{\mathrm{S}} \mathrm{F}=0.4 \bullet \mathrm{f}_{\text {EOSC }}$ EXTERNAL OSCILLATOR

Figure 12. LTC2485 Equivalent Analog Input Circuit

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For a simple approximation, the source impedance $R_{S}$ driving an analog input pin ( $\mathrm{IN}^{+}, \mathrm{IN}^{-}, \mathrm{REF}^{+}$or $\mathrm{REF}^{-}$) can be considered to form, together with $\mathrm{R}_{S W}$ and $\mathrm{C}_{\mathrm{EQ}}$ (see Figure 12), a first order passive network with a time constant $\tau=\left(R_{S}+R_{S W}\right) \bullet C_{E Q}$. The converter is able to sample the input signal with better than 1ppm accuracy if the sampling period is at least 14 times greater than the input circuit time constant $\tau$. The sampling process on the four input analog pins is quasi-independent so each time constant should be considered by itself and, under worst-case circumstances, the errors may add.

When using the internal oscillator, the LTC2485's frontend switched-capacitor network is clocked at 123 kHz corresponding to an $8.1 \mu \mathrm{~s}$ sampling period. Thus, for settling errors of less than 1ppm, the driving source impedance should be chosen such that $\tau \leq 8.1 \mu \mathrm{~s} / 14=$ 580ns. When an external oscillator of frequency $\mathrm{f}_{\text {EOSC }}$ is used, the sampling period is $2.5 / \mathrm{f}_{\text {EOSC }}$ and, for a settling error of less than 1 ppm, $\tau \leq 0.178 / f_{\text {EOSC }}$.

## Automatic Differential Input Current Cancellation

In applications where the sensor output impedance is low (up to $10 \mathrm{k} \Omega$ with no external bypass capacitor or up to $500 \Omega$ with $0.001 \mu \mathrm{~F}$ bypass), complete settling of the input occurs. In this case, no errors are introduced and direct digitization of the sensor is possible.

For many applications, the sensor output impedance combined with external bypass capacitors produces RC time constants much greater than the 580ns required for 1 ppm accuracy. For example, a $10 \mathrm{k} \Omega$ bridge driving a $0.1 \mu \mathrm{~F}$ bypass capacitor has a time constant an order of magnitudegreaterthan the required maximum. Historically, settling issues were solved using buffers. These buffers led to increased noise, reduced DC performance (Offset/ Drift), limited input/output swing (cannot digitize signals near ground or $\mathrm{V}_{\mathrm{CC}}$ ), added system cost and increased power. The LTC2485uses a proprietary switching algorithm that forces the average differential input current to zero independent of external settling errors. This allows accurate direct digitization of high impedance sensors without the need of buffers (see Figures 13 to 15). Additional errors resulting from mismatched leakage currents must also be taken into account.

The switching algorithm forces the average input current on the positive input $\left(l_{I_{N}}{ }^{+}\right)$to be equal to the average input current on the negative input $\left(l_{\mathrm{IN}}{ }^{-}\right)$. Over the complete conversion cycle, the average differential input current $\left(l_{I_{N}}{ }^{+}-\mathrm{I}_{N_{N}}\right)$ is zero. While the differential input current is zero, the common mode input current $\left(I_{I_{N}}+I_{I_{N}}^{-}\right) / 2$ is proportional to the difference between the common mode input voltage ( $\mathrm{V}_{\text {INCM }}$ ) and the common mode reference voltage (VRECM).
In applications where the input common mode voltage is equal to the reference common mode voltage, as in the case of a balance bridge type application, both the differential and common mode input current are zero. The accuracy of the converter is unaffected by settling errors. Mismatches in source impedances between IN+ and $\mathrm{IN}^{-}$also do not affect the accuracy.

In applications where the input common mode voltage is constant but different from the reference common mode voltage, the differential input current remains zero while the common mode input current is proportional to the difference between $\mathrm{V}_{\text {INCM }}$ and $\mathrm{V}_{\text {REFCM }}$. For a reference common mode of 2.5 V and an input common mode of 1.5 V , the common mode input current is approximately $0.74 \mu \mathrm{~A}$ (in simultaneous $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ rejection mode). This common mode input current has no effect on the accuracy if the external source impedances tied to $\mathrm{IN}^{+}$and $\mathrm{IN}^{-}$are matched. Mismatches in these source impedances lead to a fixed offset error but do not affect the linearity or fullscale reading. A $1 \%$ mismatch in $1 \mathrm{k} \Omega$ source resistances leads to a 15ppm shift $(74 \mu \mathrm{~V})$ in offset voltage.
In applications where the common mode input voltage varies as a function of input signal level (single-ended input, RTDs, half bridges, current sensors, etc.), the common mode input current varies proportionally with input voltage. For the case of balanced input impedances, the common mode input current effects are rejected by the large CMRR of the LTC2485 leading to little degradation in accuracy. Mismatches in source impedances lead to gain errors proportional to the difference between the common mode input voltage and the common mode reference voltage. $1 \%$ mismatches in $1 \mathrm{k} \Omega$ source resistances lead to worst-case gain errors on the order of 15ppm or 1LSB (for 1V differences in reference and input common mode

## APPLICATIONS InFORMATION

voltage). Table 6 summarizes the effects of mismatched source impedance and differences in reference/input common mode voltages.

Table 6. Suggested Input Configuration for LTC2485

|  | BALANCED INPUT RESISTANCES | UNBALANCED INPUT RESISTANCES |
| :---: | :---: | :---: |
| Constant $V_{\operatorname{IN(CM)})}-\mathrm{V}_{\text {REF(CM) }}$ | $\mathrm{C}_{\mathrm{EXT}}>1 \mathrm{nF}$ at Both $\mathrm{IN}^{+}$and $\mathrm{IN}^{-}$. Can Take Large Source Resistance with Negligible Error | $\mathrm{C}_{\mathrm{EXT}}>1 \mathrm{nF}$ at Both $\mathrm{IN}{ }^{+}$and $\mathrm{IN}^{-}$. Can Take Large Source Resistance. Unbalanced Resistance Results in an Offset Which Can be Calibrated |
| Varying $V_{\operatorname{IN(CM)}}-V_{\text {REF(CM) }}$ | $\mathrm{C}_{\mathrm{EXT}}>1 \mathrm{nF}$ at Both $\mathrm{IN}^{+}$and $\mathrm{IN}^{-}$. Can Take Large Source Resistance with Negligible Error | Minimize $\mathrm{IN}^{+}$and $\mathrm{IN}^{-}$ Capacitors and Avoid Large Source Impedance (<5k Recommended) |

The magnitude of the dynamic input current depends upon the size of the very stable internal sampling capacitors and upon the accuracy of the converter sampling clock. The accuracy of the internal clock over the entire temperature and power supply range is typically better than $0.5 \%$. Such a specification can also be easily achieved by an external clock. When relatively stable resistors ( $50 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ ) are used for the external source impedance seen by $\mathrm{IN}^{+}$and IN一, the expected drift of the dynamic current and offset will be insignificant (about 1\% of their respective values over the entire temperature and voltage range). Even for the most stringent applications, a one-time calibration operation may be sufficient.

In addition to the input sampling charge, the input ESD protection diodes have a temperature dependent leakage current. This current, nominally $1 \mathrm{nA}( \pm 10 \mathrm{nA}$ max), results in a small offset shift. A 1k source resistance will create a $1 \mu \mathrm{~V}$ typical and $10 \mu \mathrm{~V}$ maximum offset voltage.


Figure 13. An RC Network at $\operatorname{IN}{ }^{+}$and $\mathrm{IN}^{-}$


2485 F14
Figure 14. +FS Error vs RSOURCE at $\mathrm{IN}^{+}$and $\mathrm{IN}^{-}$


Figure 15. -FS Error vs RSOURCE at $\mathrm{IN}^{+}$and $\mathrm{IN}^{-}$

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## Reference Current

In a similar fashion, the LTC2485 samples the differential reference pins REF+ and REF- transferring small amount of charge to and from the external driving circuits thus producing a dynamic reference current. This current does not change the converter offset, but it may degrade the gain and INL performance. The effect of this current can be analyzed in two distinct situations.

For relatively small values of the external reference capacitors ( $\mathrm{C}_{\text {REF }}<1 \mathrm{nF}$ ), the voltage on the sampling capacitor settles almost completely and relatively large values for the source impedance result in only small errors. Such values for $\mathrm{C}_{\text {REF }}$ will deteriorate the converter offset and gain performance without significant benefits of reference filtering and the user is advised to avoid them.
Larger values of reference capacitors ( $\mathrm{C}_{\text {REF }}>1 \mathrm{nF}$ ) may be required as reference filters in certain configurations. Such capacitors will average the reference sampling charge and the external source resistance will see a quasi constant reference differential impedance.

In the following discussion, it is assumed the input and reference common mode are the same. Using internal oscillator for 60 Hz mode, the typical differential reference resistance is $1 \mathrm{M} \Omega$ which generates afull-scale $\left(\mathrm{V}_{\text {REF }} / 2\right)$ gain error of 0.51 ppm for each ohm of source resistance driving the REF ${ }^{+}$or REF ${ }^{-}$pins. For $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ mode, the related difference resistance is $1.1 \mathrm{M} \Omega$ and the resulting full-scale error is 0.46 ppm for each ohm of source resistance driving the $\mathrm{REF}^{+}$and $\mathrm{REF}^{-}$pins. For 50 Hz mode, the related difference resistance is $1.2 \mathrm{M} \Omega$ and the resulting full-scale error is 0.42 ppm for each ohm of source resistance driving the $\mathrm{REF}^{+}$and $\mathrm{REF}^{-}$pins. When $\mathrm{CAO} / \mathrm{f}_{0}$ is driven by an external oscillator with a frequency $\mathrm{f}_{\mathrm{EOSC}}$ (external conversion clock operation), the typical differential reference resistance is $0.30 \cdot 10^{12} / \mathrm{f}_{\text {EOSC }} \Omega$ and each ohm of source resistance driving the REF ${ }^{+}$or REF ${ }^{-}$pins will result in $1.67 \cdot 10^{-6}$ • $\mathrm{f}_{\mathrm{EOSC}} \mathrm{Ppm}$ gain error. The typical +FS and -FS errors for various combinations of source resistance seen by the REF $^{+}$or REF ${ }^{-}$pins and external capacitance connected to that pin are shown in Figures 16-19.

In addition to this gain error, the converter INL performance is degraded by the reference source imped-
ance. The INL is caused by the input dependent terms $-V_{I N}{ }^{2} /\left(V_{R E F} \cdot R_{E Q}\right)-\left(0.5 \cdot V_{R E F} \cdot D_{T}\right) / R_{E Q}$ in the reference pin current as expressed in Figure 12. When using internal oscillator and 60 Hz mode, every $100 \Omega$ of reference source resistance translates into about 0.67ppm additional INL error. When using internal oscillator and $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ mode, every $100 \Omega$ of reference source resistance translates into about 0.61ppm additional INL error. When using internal oscillator and 50Hz mode, every $100 \Omega$ of reference source resistance translates into about 0.56 ppm additional INL error. When $\mathrm{CAO} / \mathrm{f}_{0}$ is driven by an external oscillator with a frequency $f_{\text {EOSC }}$, every $100 \Omega$ of source resistance driving REF ${ }^{+}$or $\mathrm{REF}^{-}$translates into about $2.18 \cdot 10^{-6}$ • $\mathrm{f}_{\text {EOSC }}$ Ppm additional INL error. Figure 20 shows the typical INL error due to the source resistance driving the REF ${ }^{+}$ or REF- pins when large $C_{\text {REF }}$ values are used. The user is advised to minimize the source impedance driving the REF $^{+}$and REF ${ }^{-}$pins.

In applications where the reference and input common mode voltages are different, extra errors are introduced. For every 1 V of the reference and input common mode voltage difference ( $\mathrm{V}_{\text {REFCM }}$ - $\mathrm{V}_{\text {INCM }}$ ) and a 5 V reference, each Ohm of reference source resistance introduces an extra ( $\left.\mathrm{V}_{\text {REFCM }}-\mathrm{V}_{\text {INCM }}\right) /\left(\mathrm{V}_{\mathrm{REF}} \bullet \mathrm{R}_{\mathrm{EQ}}\right)$ full-scale gain error, which is 0.074 ppm when using internal oscillator and 60 Hz mode. When using internal oscillator and $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ mode, the extra full-scale gain error is 0.067 ppm . When using internal oscillator and 50 Hz mode, the extra gain error is 0.061 ppm. If an external clock is used, the corresponding extra gain error is $0.24 \cdot 10^{-6} \bullet f_{\text {EOSC }}$ Ppm.
The magnitude of the dynamic reference current depends upon the size of the very stable internal sampling capacitors and upon the accuracy of the converter sampling clock. The accuracy of the internal clock over the entire temperature and power supply range is typically better than $0.5 \%$. Such a specification can also be easily achieved by an external clock. When relatively stable resistors (50ppm/ ${ }^{\circ} \mathrm{C}$ ) are used for the external source impedance seen by $\mathrm{V}_{\mathrm{REF}}{ }^{+}$ and $\mathrm{V}_{\text {REF }}{ }^{-}$, the expected drift of the dynamic current gain error will be insignificant (about 1\% of its value over the entire temperature and voltage range). Even for the most stringent applications a one-time calibration operation may be sufficient.

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In addition to the reference sampling charge, the reference pins ESD protection diodes have a temperature dependent leakage current. This leakage current, nominally $1 \mathrm{nA}( \pm 10 \mathrm{nA}$ max), results in a small gain error. A $100 \Omega$ source resistance will create a $0.05 \mu \mathrm{~V}$ typical and $0.5 \mu \mathrm{~V}$ maximum full-scale error.

## Output Data Rate

When using its internal oscillator, the LTC2485 produces up to 7.5 samples per second (sps) with a notch frequency of $60 \mathrm{~Hz}, 6.25 \mathrm{sps}$ with a notch frequency of 50 Hz and 6.82 sps with the $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ rejection mode. The actual output data rate will depend upon the length of the sleep and data output phases which are controlled by the user and which can be made insignificantly short. When oper-


Figure 17. -FS Error vs R Source $^{\text {at }}$ REF $^{+}$or REF ${ }^{-}$(Small CREF )


Figure 19. -FS Error vs RSource at REF ${ }^{+}$or REF ${ }^{-}$(Large CREF )


Figure 16. +FS Error vs R Source $^{\text {at }}$ REF $^{+}$or REF ${ }^{-}$(Small CREF )


Figure 18. + FS Error vs R SOURCE at REF ${ }^{+}$or REF- ${ }^{-}$(Large C $_{\text {REF }}$ )


Figure 20. INL vs DIFFERENTIAL Input Voltage and Reference Source Resistance for $\mathrm{C}_{\text {ReF }}>1 \mu \mathrm{~F}$

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ated with an external conversion clock (CAO/foconnected to an external oscillator), the LTC2485 output data rate can be increased as desired. The duration of the conversion phase is $41036 / f_{\text {EOSC. }}$ If $\mathrm{f}_{\mathrm{EOSC}}=307.2 \mathrm{kHz}$, the converter behaves as if the internal oscillator is used and the notch is set at 60 Hz .

An increase in $f_{\text {EOSC }}$ over the nominal 307.2 kHz will translate into a proportional increase in the maximum output data rate. The increase in output rate is nevertheless accompanied by two potential effects, which must be carefully considered.

First, a change in $\mathrm{f}_{\mathrm{EOSC}}$ will result in a proportional change in the internal notch position and in a reduction of the converter differential mode rejection at the power line frequency. In many applications, the subsequent performance degradation can be substantially reduced by relying upon the LTC2485's exceptional common mode rejection and by carefully eliminating common mode to differential mode conversion sources in the input circuit. The user should avoid single-ended input filters and should maintain a very high degree of matching and symmetry in the circuits driving the $\mathrm{IN}^{+}$and $\mathrm{IN}^{-}$pins.

Second, the increase in clock frequency will increase proportionally the amount of sampling charge transferred through the input and the reference pins. If large external input and/or reference capacitors ( $\mathrm{C}_{\mathrm{IN}}, \mathrm{C}_{\text {REF }}$ ) are used,


2485 F21
Figure 21. Offset Error vs Output Data Rate and Temperature
the previous section provides formulae for evaluating the effect of the source resistance upon the converter performance for any value of $f_{\text {EOSC }}$. If small external input and/ or reference capacitors ( $\mathrm{C}_{\mathrm{IN}_{N}}, \mathrm{C}_{\text {REF }}$ ) are used, the effect of the external source resistance upon the LTC2485 typical performance can be inferred from Figures 14, 15, 16 and 17 in which the horizontal axis is scaled by 307200/f EOSC.
Typical measured performance curves for output data rates up to 25 readings per second are shown in Figures 21 to 28. In order to obtain the highest possible level of accuracy from this converter at output data rates above 20 readings per second, the user is advised to maximize the power supply voltage used and to limit the maximum ambient operating temperature. In certain circumstances, a reduction of the differential reference voltage may be beneficial.

## Input Bandwidth

The combined effect of the internal SINC $^{4}$ digital filter and of the analog and digital auto-calibration circuits determines the LTC2485 input bandwidth. When the internal oscillator is used with the notch set at 60 Hz , the 3 dB input bandwidth is 3.63 Hz . When the internal oscillator is used with the notch set at 50 Hz , the 3 dB input bandwidth is 3.02 Hz . If an external conversion clock generator of frequency $\mathrm{f}_{\text {EOSC }}$ is connected to the $\mathrm{CAO} / \mathrm{f}_{0}$ pin, the 3 dB input bandwidth is $11.8 \cdot 10^{-6} \cdot f_{\text {EOSC }}$.


2485 F22
Figure 22. +FS Error vs Output Data Rate and Temperature

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2485 F23
Figure 23. -FS Error vs Output Data Rate and Temperature


2485 F25
Figure 25. Resolution (INL ${ }_{\text {MAX }} \leq 1 \mathrm{LSB}$ ) vs Output Data Rate and Temperature


2485 F27
Figure 27. Resolution (Noise ${ }_{\text {RMS }} \leq$ 1LSB) vs Output Data Rate and Reference Voltage


2485 F24
Figure 24. Resolution ( Noise $_{\text {RMS }} \leq 1$ 1LSB) vs Output Data Rate and Temperature


2485 F26
Figure 26. Offset Error vs Output Data Rate and Reference Voltage


2485 F28
Figure 28. Resolution (INL ${ }_{\text {MAX }} \leq 1 L S B$ )
vs Output Data Rate and Reference Voltage

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Due to the complex filtering and calibration algorithms utilized, the converter input bandwidth is not modeled very accurately by a first order filter with the pole located at the 3 dB frequency. When the internal oscillator is used, the shape of the LTC2485 input bandwidth is shown in Figure 29. When an external oscillator of frequency $f_{\text {EOSC }}$ is used, the shape of the LTC2485 input bandwidth can be derived from Figure $29,60 \mathrm{~Hz}$ mode curve in which the horizontal axis is scaled by $\mathrm{f}_{\mathrm{EOSC}} / 307200$.
The conversion noise $\left(600 \mathrm{nV}_{\text {RMS }}\right.$ typical for $\mathrm{V}_{\text {REF }}=5 \mathrm{~V}$ ) can be modeled by a white noise source connected to a noise free converter. The noise spectral density is $47 \mathrm{nV} \sqrt{\mathrm{Hz}}$ for an infinite bandwidth source and $64 \mathrm{nV} \sqrt{\mathrm{Hz}}$ for a single 0.5 MHz pole source. From these numbers, it is clear that particular attention must be given to the design of external amplification circuits. Such circuits face the simultaneous requirements of very low bandwidth (just a few Hz) in order to reduce the output referred noise and relatively high bandwidth (at least 500 kHz ) necessary to drive the input switched-capacitor network. A possible solution is a high gain, low bandwidth amplifier stage followed by a high bandwidth unity-gain buffer.
When external amplifiers are driving the LTC2485, the ADC input referred system noise calculation can be simplified by Figure 30. The noise of an amplifier driving the LTC2485 input pin can be modeled as a band limited white noise source. Its bandwidth can be approximated by the bandwidth of a single pole lowpass filter with a corner frequency $f_{\mathrm{i}}$. The amplifier noise spectral density is $n_{i}$. From Figure 30, using $f_{i}$ as the $x$-axis selector, we can find on the $y$-axis the noise equivalent bandwidth freq ${ }_{i}$ of the input driving amplifier. This bandwidth includes the band limiting effects of the ADC internal calibration and filtering. The noise of the driving amplifier referred to the converter input and including all these effects can be calculated as $N=n_{i} \bullet \sqrt{f r e q} \mathrm{q}_{\mathrm{i}}$. The total system noise (referred to the LTC2485 input) can now be obtained by summing as square root of sum of squares the three ADC input referred noise sources: the LTC2485 internal noise, the noise of the $\operatorname{IN}{ }^{+}$driving amplifier and the noise of the $\mathrm{IN}^{-}$driving amplifier.

If the $C A O / f_{0}$ pin is driven by an external oscillator of frequency $\mathrm{f}_{\mathrm{EOSC}}$, Figure 30 can still be used for noise calculation if the $x$-axis is scaled by $\mathrm{f}_{\mathrm{EOSC}} / 307200$. For large values of the ratio $\mathrm{f}_{\mathrm{EOSC}} / 307200$, the Figure 30 plot accuracy begins to decrease, but at the same time the LTC2485 noise floor rises and the noise contribution of the driving amplifiers lose significance.

## Normal Mode Rejection and Anti-Aliasing

One of the advantages delta-sigma ADCs offer over conventional ADCs is on-chip digital filtering. Combined with a large oversampling ratio, the LTC2485 significantly simplifies anti-aliasing filter requirements. Additionally, the input current cancellation feature of the LTC2485 allows external lowpass filtering without degrading the DC performance of the device.
The SINC ${ }^{4}$ digital filter provides greaterthan 120 dB normal mode rejection at all frequencies except DC and integer multiples of the modulator sampling frequency ( $\mathrm{f}_{\mathrm{S}}$ ). The LTC2485's aut0-calibration circuits further simplify the anti-aliasing requirements by additional normal mode signal filtering both in the analog and digital domain. Independent of the operating mode, $\mathrm{f}_{\mathrm{S}}=256 \bullet \mathrm{f}_{\mathrm{N}}=2048$ - $f_{\text {OUTMAX }}$ where $f_{N}$ is the notch frequency and $f_{\text {OUtMax }}$ is the maximum output data rate. In the internal oscillator mode with a 50 Hz notch setting, $\mathrm{f}_{\mathrm{S}}=12800 \mathrm{~Hz}$, with $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ rejection, $\mathrm{f}_{\mathrm{S}}=13960 \mathrm{~Hz}$ and with a 60 Hz notch setting $\mathrm{f}_{\mathrm{S}}=15360 \mathrm{~Hz}$. In the external oscillator mode, $\mathrm{f}_{\mathrm{S}}=$ $\mathrm{f}_{\mathrm{EOSC}} / 20$. The performance of the normal mode rejection is shown in Figures 31 and 32.
In 1x speed mode, the regions of low rejection occurring at integer multiples of $f_{S}$ have a very narrow bandwidth. Magnified details of the normal mode rejection curves are shown in Figure 33 (rejection near DC) and Figure 34 (rejection at $\mathrm{f}_{\mathrm{S}}=256 \mathrm{f}_{\mathrm{N}}$ ) where $\mathrm{f}_{\mathrm{N}}$ represents the notch frequency. These curves have been derived for the external oscillator mode but they can be used in all operating modes by appropriately selecting the $\mathrm{f}_{\mathrm{N}}$ value.

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2485 F29
Figure 29. Input Signal Using the Internal Oscillator


2485 F31
Figure 31. Input Normal Mode Rejection, Internal Oscillator and 50Hz Notch Mode


2485 F33
Figure 33. Input Normal Mode Rejection at DC


Figure 30. Input Referred Noise Equivalent Bandwidth of an Input Connected White Noise Source


Figure 32. Input Normal Mode Rejection at DC


Figure 34. Input Normal Mode Rejection at $\mathrm{f}_{\mathrm{s}}=256 \mathrm{f}_{\mathrm{N}}$

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The user can expect to achieve this level of performance using the internal oscillator as it is demonstrated by Figures 35, 36 and 37 . Typical measured values of the normal mode rejection of the LTC2485 operating with an internal oscillator and a 60 Hz notch setting are shown in Figure 35 superimposed over the theoretical calculated curve. Similarly, the measured normal mode rejection of the LTC2485 for the 50 Hz rejection mode and $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ rejection mode are shown in Figures 36 and 37.
As a result of these remarkable normal mode specifications, minimal (if any) anti-alias filtering is required in front of the LTC2485. If passive RC components are placed in front of the LTC2485, the input dynamic current should be considered (see Input Current section). In this case, the differential input current cancellation feature of the LTC2485 allows external RC networks without significant degradation in DC performance.
Traditional high order delta-sigma modulators, while providing very good linearity and resolution, suffer from potential instabilities at large input signal levels. The proprietary architecture used for the LTC2485 third
order modulator resolves this problem and guarantees a predictable stable behavior at input signal levels of up to $150 \%$ of full-scale. In many industrial applications, it is not uncommon to have to measure microvolt level signals superimposed on volt level perturbations and the LTC2485 is eminently suited for such tasks. When the perturbation is differential, the specification of interest is the normal mode rejection for large input signal levels. With a reference voltage $\mathrm{V}_{\text {REF }}=5 \mathrm{~V}$, the LTC2485 has a full-scale differential input range of 5 V peak-to-peak. Figures 38 and 39 show measurement results for the LTC2485 normal mode rejection ratio with a 7.5 V peak-to-peak ( $150 \%$ of full scale) input signal superimposed over the more traditional normal mode rejection ratio results obtained with a 5 V peak-to-peak (full-scale) input signal. In Figure 38, the LTC2485 uses the internal oscillator with the notch set at 60 Hz and in Figure 39 it uses the internal oscillator with the notch set at 50 Hz . It is clear that the LTC2485 rejection performance is maintained with no compromises in this extreme situation. When operating with large input signal levels, the user must observe that such signals do not violate the device absolute maximum ratings.

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Figure 35. Input Normal Mode Rejection vs Input Frequency with Input Perturbation of $100 \%$ Full-Scale ( 60 Hz Notch)


Figure 36. Input Normal Mode Rejection vs Input Frequency with Input Perturbation of $100 \%$ Full-Scale ( 50 Hz Notch)


Figure 37. Input Normal Mode Rejection vs Input Frequency with Input Perturbation of $100 \%$ Full-Scale ( $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ Mode)


Figure 38. Measured Input Normal Mode Rejection vs Input Frequency with Input Perturbation of 150\% Full-Scale (60Hz Notch)


Figure 39. Measured Input Normal Mode Rejection vs Input Frequency with Input Perturbation of 150\% Full-Scale (50Hz Notch)

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Using the $2 x$ speed mode of the LTC2485, the device bypasses the digital offset calibration operation to double the output data rate. The superior normal mode rejection is maintained as shown in Figures 31 and 32. However, the magnified details near $D C$ and $f_{S}=256 f_{N}$ are different, see Figures 40 and 41 . In $2 x$ speed mode, the bandwidth is 11.4 Hz for the 50 Hz rejection mode, 13.6 Hz for the 60 Hz rejection mode and 12.4 Hz for the $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ rejection mode. Typical measured values of the normal mode rejection of the LTC2485 operating with the internal oscillator and $2 x$ speed mode is shown in Figure 42.

When the LTC2485 is configured in $2 x$ speed mode, by performing a running average, a SINC ${ }^{1}$ notch is combined with the SINC ${ }^{4}$ digital filter, yielding the normal mode rejection identical as that for the 1 x speed mode. The averaging operation still keeps the output rate with the following algorithm:

Result 1 = average (sample 0, sample 1)
Result 2 = average (sample 1, sample 2)

## Result $\mathrm{n}=$ average (sample $\mathrm{n}-1$, sample n )

The main advantage of the running average is that it achieves simultaneous $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ rejection at twice the effective output rate, as shown in Figure 43. The raw output data provides a better than 70dB rejection over 48 Hz to 62.4 Hz , which covers both $50 \mathrm{~Hz} \pm 2 \%$ and $60 \mathrm{~Hz} \pm 2 \%$. With running average on, the rejection is better than 87 dB for both $50 \mathrm{~Hz} \pm 2 \%$ and $60 \mathrm{~Hz} \pm 2 \%$.

## Complete Thermocouple Measurement System with Cold Junction Compensation

The LTC2485 is ideal for direct digitization of thermocouples and other low voltage output sensors. The input has a typical offset error of $500 \mathrm{nV}(2.5 \mu \mathrm{~V}$ max) offset drift of $10 \mathrm{nV} /{ }^{\circ} \mathrm{C}$ and a noise level of 600 nV RMS.
Figure 45 (last page of this data sheet) is a complete type K thermocouple meter. The only signal conditioning is a simple surge protection network. In any thermocouple meter, the cold junction temperature sensor must be at the same temperature as the junction between the thermocouple materials and the copper printed circuit board traces. The tiny LTC2485 can be tucked neatly underneath an Omega MPJ-K-F thermocouple socket ensuring close thermal coupling.
The LTC2485's $1.4 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ PTAT circuit measures the cold junction temperature. Once the thermocouple voltage and cold junction temperature are known, there are many ways of calculating the thermocouple temperature including a straight-line approximation, lookup tables or a polynomial curve fit. Calibration is performed by applying an accurate 500 mV to the ADC input derived from an LT®1236 reference and measuring the local temperature with an accurate thermometer as shown in Figure 44. In calibration mode, the up and down buttons are used to adjust the local temperature reading until it matches an accurate thermometer. Both the voltage and temperature calibration are easily automated.

The complete microcontroller code for this application is available on the LTC2485 product webpage at:
http://www.linear.com
It can be used as a template for may different instruments and it illustrates how to generate calibration coefficients for the onboard temperature sensor. Extensive comments detail the operation of the program. The read_LTC2485() function controls the operation of the LTC2485 and is listed below for reference.

## APPLICATIONS INFORMATION



2485 F40
Figure 40. Input Normal Mode Rejection 2x Speed Mode


2485 F42
Figure 42. Input Normal Mode Rejection vs Input Frequency, 2x Speed Mode and 50Hz/60Hz Mode


Figure 41. Input Normal Mode Rejection 2x Speed Mode


2485 F43
Figure 43. Input Normal Mode Rejection 2x Speed Mode


Figure 44. Calibration Setup

## APPLICATIONS INFORMATION

```
/*
LTC248X.h
Processor setup and
Lots of useful defines for configuring the LTC2481, LTC2483, and LTC2485.
* /
#include <16F73.h> // Device
#use delay(clock=6000000) // 6MHz clock
//#fuses NOWDT,HS, PUT, NOPROTECT, NOBROWNOUT // Configuration fuses
#rom 0x2007={0x3F3A} // Equivalent and more reliable fuse config.
#use I2C(master, sda=PIN_C5, scl=PIN_C3, SLOW)// Set up i2c port
#include "PCM73A.h" / - Various defines
#include "lcd.c" // LCD driver functions
#define READ 0x01 // bitwise OR with address for read or write
#define WRITE 0x00
#define LTC248XADDR 0b01001000 // The one and only LTC248X in this circuit,
// with both address lines floating.
// Useful defines for the LTC2481 and LTC2485 - OR them together to make the
// 8 bit config word.
// These do NOT apply to the LTC2483.
// Select gain - 1 to 256 (also depends on speed setting)
// Does NOT apply to LTC2485.
\#define GAIN1 0b00000000 \(/ / G=1 \quad(S P D=0), G=1 \quad(S P D=1)\)
\#define GAIN2 0b00100000 \(/ / G=4 \quad(S P D=0), G=2 \quad(S P D=1)\)
\#define GAIN3 0b01000000 \(/ / / G=8 \quad(S P D=0), G=4 \quad(S P D=1)\)
\#define GAIN4 0b01100000 \(/ / G=16 \quad(S P D=0), G=8 \quad(S P D=1)\)
\#define GAIN5 0b10000000 \(/ / G=32 \quad(S P D=0), G=16 \quad(S P D=1)\)
\#define GAIN6 0b10100000 \(/ / G=64 \quad(S P D=0), G=32 \quad(S P D=1)\)
\#define GAIN7 0b11000000 \(/ / G=128(S P D=0), G=64 \quad(S P D=1)\)
\#define GAIN8 0b11100000 \(/ / G=256(S P D=0), G=128(S P D=1)\)
// Select ADC source - differential input or PTAT circuit
\#define VIN 0b00000000
\#define PTAT 0b00001000
// Select rejection frequency - 50, 55, or 60 Hz
\#define R50 0b00000010
\#define R55 0b00000000
\#define R60 0b00000100
// Select speed mode
\#define SLOW 0b00000000 // slow output rate with autozero
\#define FAST 0b00000001 // fast output rate with no autozero
```


## APPLICATIONS INFORMATION

```
/*
LTC2485.c
Basic voltmeter test program for LTC2485
Reads LTC2485, converts result to volts,
and prints voltage to a 2 line by 16 character LCD display.
Mark Thoren
Linear Technology Corporation
June 23, 2005
Written for CCS PCM compiler, Version 3.182
*/
#include "LTC248X.h"
/*** read LTC2485() ************************************************************
This is the function that actually does all the work of talking to the LTC2485.
Arguments: addr - device address
    config - configuration bits for next conversion
Returns: zero if conversion is in progress,
    3 2 ~ b i t ~ s i g n e d ~ i n t e g e r ~ L T C 2 4 8 5 ~ o u t p u t ~ w o r d . ~
the i2c_xxxx() functions do the following:
void i2c start(void): generate an i2c start or repeat start condition
void i2c_stop(void): generate an i2c stop condition
char i2c read(boolean): return 8 bit i2c data while generating an ack or nack
boolean ì2c_write(): send 8 bit i2c data and return ack or nack from slave device
These functions are very compiler specific, and can use either a hardware i2c
port or software emulation of an i2c port. This example uses software emulation.
A good starting point when porting to other processors is to write your own
i2c functions. Note that each processor has its own way of configuring
the i2c port, and different compilers may or may not have built-in functions
for the i2c port.
When in doubt, you can always write a "bit bang" function for troubleshooting purposes.
The "fourbytes" structure allows byte access to the 32 bit return value:
```

```
struct fourbytes // Define structure of four consecutive bytes
```

struct fourbytes // Define structure of four consecutive bytes
int8 te0;
int8 te0;
int8 te1;
int8 te1;
int8 te2; // also work, but a union of 4 bytes and a 32 bit int
int8 te2; // also work, but a union of 4 bytes and a 32 bit int
int8 te3; // is probably more portable.
int8 te3; // is probably more portable.
};

```
    };
```


## LTC2485

## APPLICATIONS INFORMATION

```
*****************************************************************************************/
signed int32 read_LTC2485(char addr, char config)
    {
    struct fourbytes // Define structure of four consecutive bytes
        { // To allow byte access to a 32 bit int or float.
        int8 te0; //
        int8 te1; // The make32() function in this compiler will
        int8 te2; // also work, but a union of 4 bytes and a 32 bit int
        int8 te3; // is probably more portable.
        };
    union // adc_code.bits32 all 32 bits
    { // adc_code.by.te0 byte 0
    signed int32 bits32; // adc_code.by.te1 byte 1
    struct fourbytes by; // adc_code.by.te2 byte 2
    } adc_code; // adc_code.by.te3 byte 3
// Start communication with LTC2485:
    i2c_start();
    if(i2c_write(addr | WRITE))// If no acknowledge, return zero
            {
            i2c_stop();
            retūrn 0;
            }
        i2c_write(config);
        i2c-start();
        i2c_write(addr | READ);
        adc-code.by.te3 = i2c read();
        adc_code.by.te2 = i2c_read();
        adc_code.by.te1 = i2c_read();
        adc_code.by.te0 = i2c_read();
        i2c_stop();
    return -adc code.bits32;
    } // End o\overline{f read_LTC2485()}
/*** initialize()
Basic hardware initialization of controller and LCD, send Hello message to LCD
```

```
void initialize(void)
```

void initialize(void)
{
{
// General initialization stuff.
// General initialization stuff.
setup_adc_ports(NO_ANALOGS);
setup_adc_ports(NO_ANALOGS);
setup_adc(ADC_OFF);
setup_adc(ADC_OFF);
setup_counters}(RTCC_INTERNAL,RTCC_DIV_1);
setup_counters}(RTCC_INTERNAL,RTCC_DIV_1);
setup_timer_1(T1_DISABLED);
setup_timer_1(T1_DISABLED);
setup_timer_2(T2_DISABLED,0,1);
setup_timer_2(T2_DISABLED,0,1);
lcd_init(); // Initialize LCD
lcd_init(); // Initialize LCD
delāy_ms(6);
delāy_ms(6);
printf(lcd_putc, "Hello!"); // Obligatory hello message
printf(lcd_putc, "Hello!"); // Obligatory hello message
delay ms(5\overline{0}0); // for half a second
delay ms(5\overline{0}0); // for half a second
} // End of initialize()

```
    } // End of initialize()
```


## APPLICATIONS InFORMATION

```
/*** main() ***************************************************************************
Main program initializes microcontroller registers, then reads the LTC2481
repeatedly
void main()
    {
    signed int32 x, y; // Integer result from LTC2481
    float voltage; // Variable for floating point math
    int16 timeout;
    initialize(); // Hardware initialization
    while(1)
        {
        delay_ms(1); // Pace the main loop to something more than 1 ms
// This is a basic error detection scheme. The LTC2485 will never take more than
// 163.5ms, 149.9ms, or 136.5ms to complete a conversion in the 50Hz, 55Hz, and 60Hz
// rejection modes, respectively.
// If read LTC2485() does not return non-zero within this time period, something
// is wrong}, such as an incorrect i2c address or bus conflict
    if((x = read_LTC2485(LTC248XADDR, VIN | R50 | SLOW)) != 0)
        {
            // No timeout, everything is okay
            timeout = 0; // reset timer
            x ^= 0x80000000; // Invert MSB, result is 2's complement
            voltage = (float) x; // convert to float
            voltage = voltage * 5.0 / 2147483648.0;// Multiply by Vref, divide by 2^31
            lcd_putc('\f'); // Clear screen
            lcd_gotoxy(1,1); // Goto home position
            prin̄tf(lcd_putc, "%01.6f", voltage); // Display voltage
            }
        else
            {
            ++timeout;
            }
        if(timeout > 200)
            {
            timeout = 200; // Prevent rollover
            lcd_gotoxy(1,1);
            prin̄tf(lcd putc, "ERROR - TIMEOUT");
            delay_ms(500);
            }
        } // End of main loop
    } // End of main()
```


## PACKAGE DESCRIPTION

Please refer to http://www.linear.com/designtools/packaging/ for the most recent package drawings.

## DD Package

10-Lead Plastic DFN (3mm $\times 3 \mathrm{~mm}$ )
(Reference LTC DWG \# 05-08-1699 Rev C)


RECOMMENDED SOLDER PAD PITCH AND DIMENSIONS


NOTE:

1. DRAWING TO BE MADE A JEDEC PACKAGE OUTLINE MO-229 VARIATION OF (WEED-2). CHECK THE LTC WEBSITE DATA SHEET FOR CURRENT STATUS OF VARIATION ASSIGNMENT 2. DRAWING NOT TO SCALE
2. ALL DIMENSIONS ARE IN MILLIMETERS
3. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE

MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15 mm ON ANY SIDE
5. EXPOSED PAD SHALL BE SOLDER PLATED
6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION ON THE TOP AND BOTTOM OF PACKAGE

## REVISION HISTORY (Revision history begins at Rev B)

| REV | DATE | DESCRIPTION | PAGE NUMBER |
| :---: | :---: | :--- | :---: |
| B | $11 / 09$ | Update Tables 2 and 3 | 15 |
| C | $7 / 10$ | Revised Typical Application drawing <br> Added text to I 2 C Interface section | 1 |
| D | $10 / 14$ | Clarified performance vs $\mathrm{f}_{0}$ frequency, reduced external oscillator maximum frequency to $1 \mathrm{MHz}$. <br> Clarified temperature sensor performance. <br> Added underrange note to Table 3. | $5,8,26,27$ |

## TYPICAL APPLICATION



Figure 45. Complete Type K Thermocouple Meter

## RELATED PARTS

| PART NUMBER | DESCRIPTION | COMMENTS |
| :---: | :---: | :---: |
| LT1236A-5 | Precision Bandgap Reference, 5V | 0.05\% Max Initial Accuracy, 5ppm/ ${ }^{\circ} \mathrm{C}$ Drift |
| LT1460 | Micropower Series Reference | 0.075\% Max Initial Accuracy, 10ppm/ ${ }^{\circ} \mathrm{C}$ Max Drift |
| LT1790 | Micropower SOT-23 Low Dropout Reference Family | 0.05\% Max Initial Accuracy, 10ppm/ ${ }^{\circ} \mathrm{C}$ Max Drift |
| LTC2400 | 24-Bit, No Latency $\triangle \Sigma$ ADC in S0-8 | 0.3ppm Noise, 4ppm INL, 10ppm Total Unadjusted Error, $200 \mu \mathrm{~A}$ |
| LTC2410 | 24-Bit, No Latency $\triangle \Sigma$ ADC with Differential Inputs | $0.8 \mu \mathrm{~V}_{\text {RMS }}$ Noise, 2ppm INL |
| LTC2411/LTC2411-1 | 24 -Bit, No Latency $\triangle \Sigma$ ADCs with Differential Inputs in MSOP | $1.45 \mu \mathrm{~V}$ RMS Noise, 4 ppm INL, Simultaneous $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ Rejection (LTC2411-1) |
| LTC2413 | 24-Bit, No Latency $\triangle \Sigma$ ADC with Differential Inputs | Simultaneous 50Hz/60Hz Rejection, $800 \mathrm{nV} \mathrm{R}_{\text {RMS }}$ Noise |
| LTC2415/LTC2415-1 | 24-Bit, No Latency $\triangle \Sigma$ ADCs with 15 Hz Output Rate | Pin Compatible with the LTC2410 |
| LTC2414/LTC2418 | 8-/16-Channel 24-Bit, No Latency $\triangle \Sigma$ ADCs | 0.2ppm Noise, 2ppm INL, 3ppm Total Unadjusted Errors 200ヶA |
| LTC2440 | High Speed, Low Noise 24-Bit $\Delta \Sigma$ ADC | 3.5kHz Output Rate, 200nV Noise, 24.6 ENOBs |
| LTC2480 | 16-Bit $\Delta \Sigma$ ADC with Easy Drive Inputs, 600 nV Noise, Programmable Gain, and Temperature Sensor | Pin Compatible with LTC2482/LTC2484 |
| LTC2481 | 16-Bit $\Delta \Sigma$ ADC with Easy Drive Inputs, 600 nV Noise, $I^{2} \mathrm{C}$ Interface, Programmable Gain, and Temperature Sensor | Pin Compatible with LTC2483/LTC2485 |
| LTC2482 | 16-Bit $\triangle \Sigma$ ADC with Easy Drive Inputs | Pin Compatible with LTC2480/LTC2484 |
| LTC2483 | 16 -Bit $\triangle \Sigma$ ADC with Easy Drive Inputs, and $\mathrm{I}^{2} \mathrm{C}$ Interface | Pin Compatible with LTC2481/LTC2485 |
| LTC2484 | $24-$ Bit $\Delta \Sigma$ ADC with Easy Drive Inputs | Pin Compatible with LTC2480/LTC2482 |
| 2485 fd |  |  |

